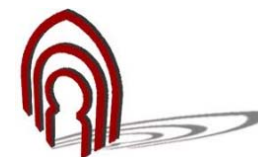


COMPOSITE MEMBRANES FOR HIGH TEMPERATURE PEM FUEL CELLS: FROM SINGLE CELLS TO STACK



M.A. Rodrigo, J. Lobato, P. Cañizares, F.J. Pinar, H. Zamora and D. Úbeda
University of Castilla-La Mancha, Chemical Engineering Department, Building
Enrique Costa Novella, Av. Camilo José Cela nº12. 13071. Ciudad Real, (Spain) e-
mail: manuel.rodrigo@uclm.es; tel: +34 902204100 ext:3411.





► Introduction

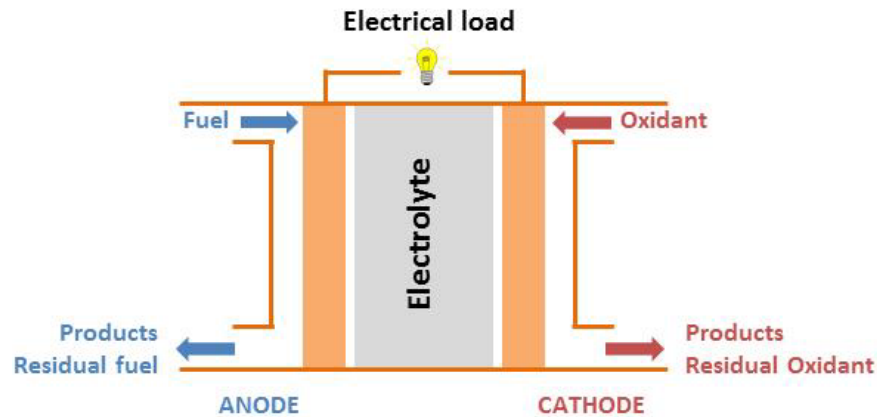
Objetives

Results and discussion

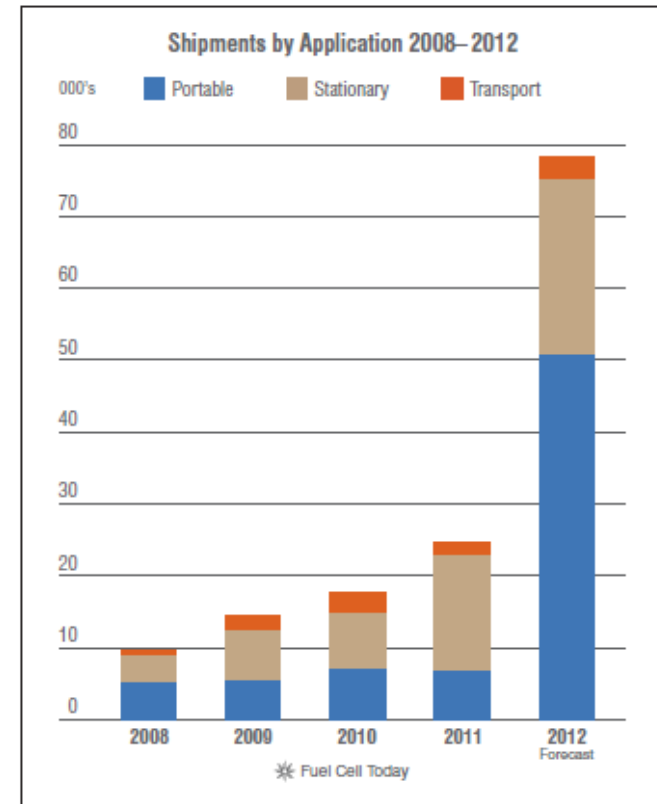
Conclusions

Acknowledgements



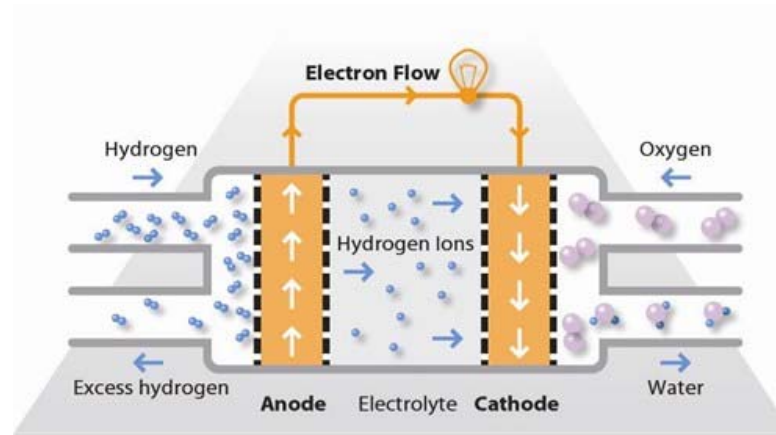


Device that converts the **CHEMICAL** energy of a fuel and a comburent **DIRECTLY** into **ELECTRIC** energy and **HEAT**



FUEL CELLS

- ✓ Polymer Electrolyte Membrane Fuel Cell (PEMFC)
- ✓ Phosphoric Acid Fuel Cell (PAFC)
- ✓ Alkaline Fuel Cell (AFC)
- ✓ Solid Oxide Fuel Cells (SOFC)
- ✓ Molten Carbonates Fuel Cell (MCFC)



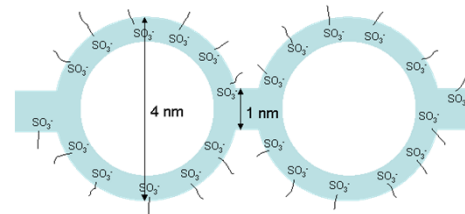
PEMFC



Most Extended Material

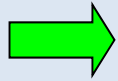


NAFION



Perfluorosulphonic Acid Membrane

Proton
Conductivity
 \propto
Water Content



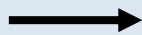
Humidification
 $T < 90\text{ }^{\circ}\text{C}$



- Sluggish kinetic of the cathodic reaction
- Low tolerance to fuel impurities



ALTERNATIVE

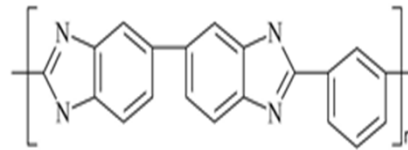


INCREASE OPERATIONAL TEMPERATURE
 $(T \approx 100\text{-}200\text{ }^{\circ}\text{C})$

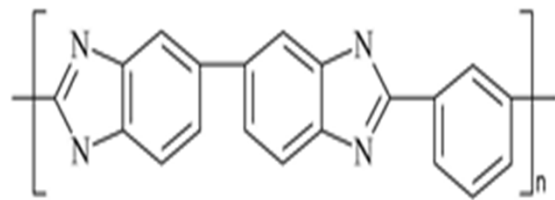
Polymeric Material

- ✓ Thermal and Mechanical Resistance
- ✓ Proton Conduction

**PBI AS
ELECTROLYTE
MATERIAL FOR HT-
PEMFC**

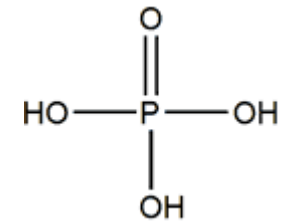


- Excellent thermal resistance (> 550 °C in air)
- Low methanol crossover compared to Nafion[®]
- Acceptable mechanical properties
- No needs feed stream humidification



PBI

+



H₃PO₄



↑ **Conductivity**

- ✓ High conductivity when doped with H₃PO₄ up to 200 °C



↓ **Mechanical Properties**

↓ **FC Stability vs. Time**

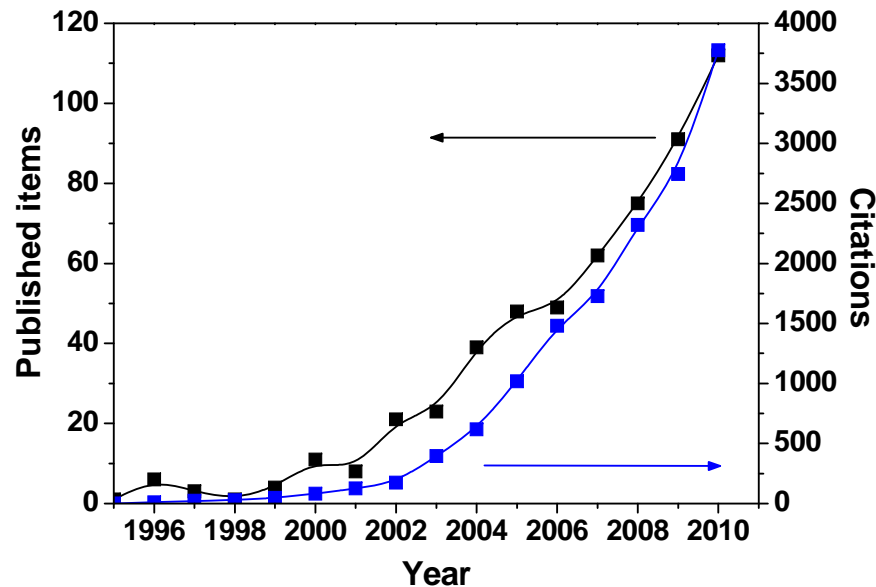
- ✓ Membrane becomes more plastic
- ✓ Acid leaching to electrodes → Electrodes deterioration
- ✓ ...

Conventional PEM Fuel Cells

- Nafion
- Operating T: ~ 80 °C
 - ✓ Rapid start/stop
 - ✓ Higher durability

High temperature PEM Fuel Cells

- H_3PO_4 -doped PBI
- Operating T: ~ 150 °C
 - ✓ Easier water management
 - ✓ Catalyst less sensitive to poisons
 - ✓ Waste heat recovery



*Number of published item and citations per year of the topic
"polybenzimidazole" and "fuel cell" classified within Web of Knowledge*

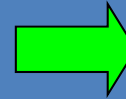


Main drawback of PBI-
HTPEMFC:

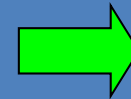
**HIGH CELL VOLTAGE
DEGRADATION RATE**

MAIN
DEGRADATION
MECHANISMS
IDENTIFIED

- Leach of acid
- Catalyst sintering and agglomeration



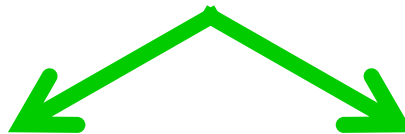
MEMBRANE
ELECTROLYTE
ENHANCEMENT



CATALYST
ENHANCEMENT

**CATALYST
PROPERTIES
ENHANCEMENT**

**MEMBRANE
ELECTROLYTE
PROPERTIES
ENHANCEMENT**



Service lifetime increase

Performance increase



Introduction

► Objectives

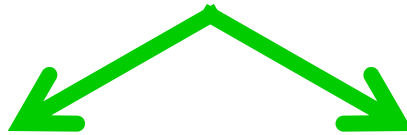
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MEMBRANE ELECTROLYTE PROPERTIES ENHANCEMENT



Service lifetime increase

Performance increase



- ✓ Performance enhancement: how to obtain better membranes for HTPEMFC in order to **increase service lifetime** and **get a better performance**?
- ✓ Scale up concerns: **Does size matter**?
- ✓ Lack of reproducibility concerns: How to obtain better **reproducibilities**?

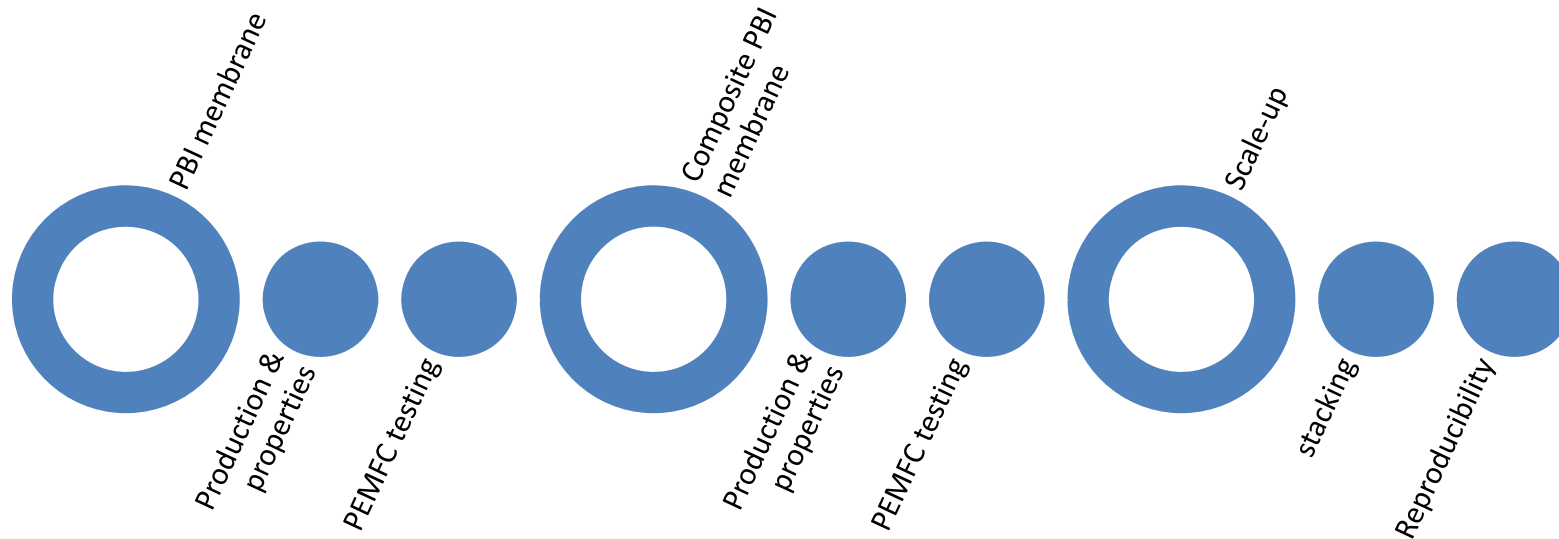
Develop PBI synthesis routes and scale-up the production capacity per batch in order to obtain large amounts of polymer for preparing membranes with uniform properties

Study simple PBI based HT-PEMFC to assess performance in terms of power produced and lifetime

Develop composite membranes by physical modification of the membrane structure with the addition of inorganic fillers with high water and acid retention capability and compare performance with single PBI based membranes

Scale-up the standard PBI membrane and the composite membrane FTPEMFC. From 5 to 50 cm² membrane area and from single to a 3 FC stack (150 cm²)

Evaluation of the current and composition distribution to check for main causes of rapid decay





Introduction

Objetives

► **Results and discussion**

Conclusions

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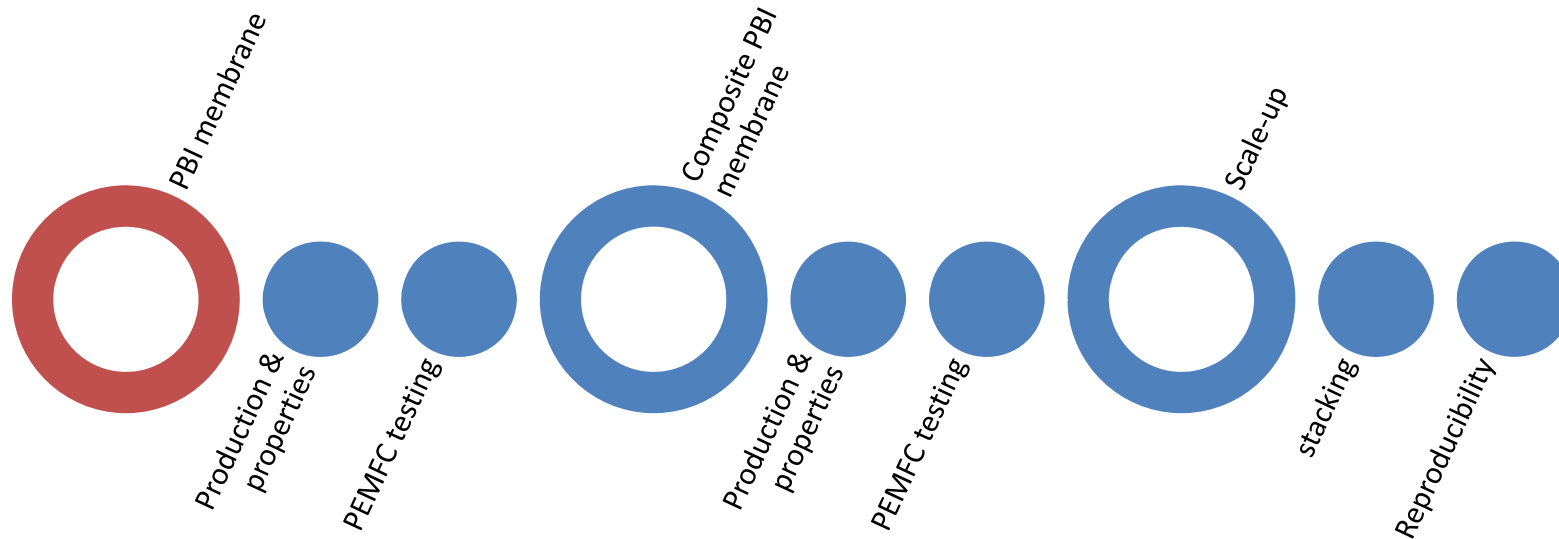
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Is it difficult to obtain the polymer to cast PBI membranes?



Previous remarks about PBI

Typical intrinsic viscosity of commercial PBI is around 0.8 (meaning molecular weights of around 140000 Daltons). **It is not designed for PEMFC application but for textile and chemicals production!!!!**



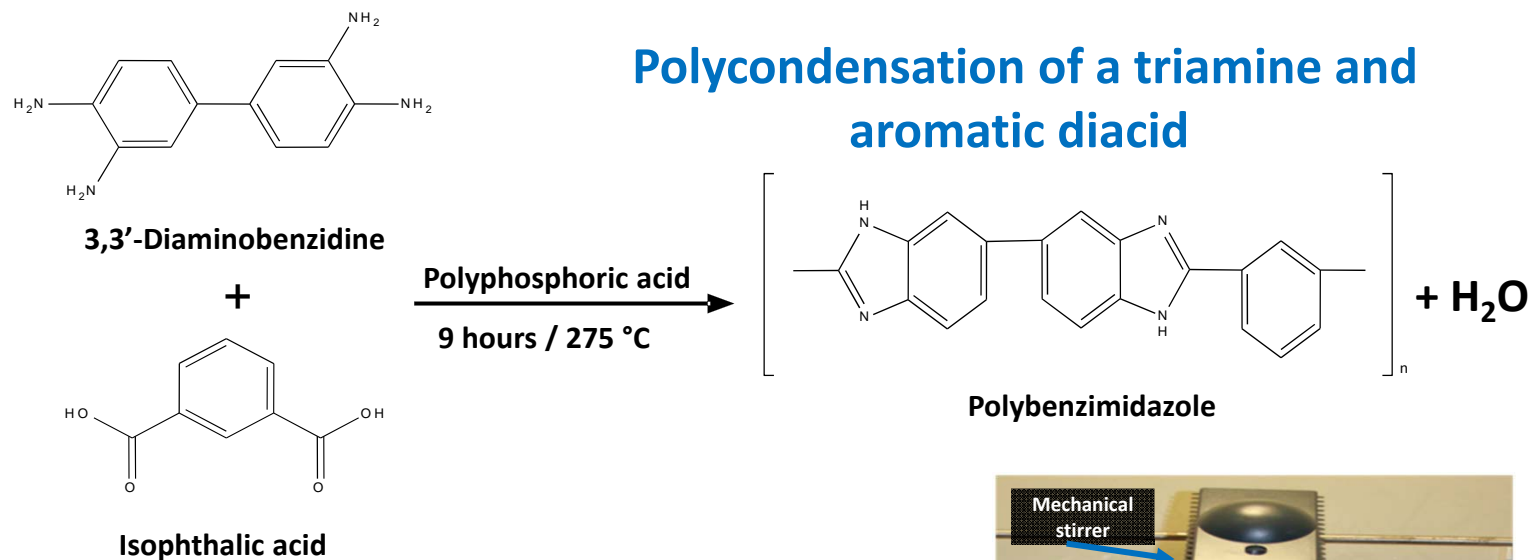
Very high molecular weights lead to insolubility of polymer but low molecular weights lead to bad mechanical properties. **Optimum value: 1.8-2.0 (according to our experience)**



We have to develop our own synthesis route!

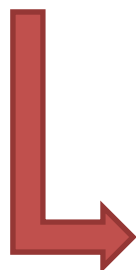


Procedure for manufacturing PBI



USE OF SYNTHESIS METHOD FROM PREVIOUS STUDIES

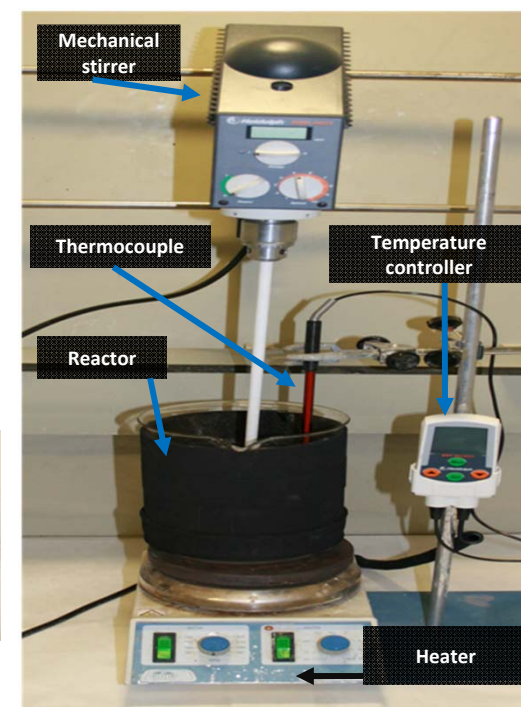
Difficulties in mixing stages: HIGH VISCOSITY



≠



POLYMER QUALITY



First batches results:

- ✓ Sized for 4.5 g/batch. Only around 700 cm² membranes (50 μm thickness)/ batch (drawback for a later comparison of performance of HTPEMFC)
- ✓ Many experimental difficulties during the polymerization
- ✓ Not very high reproducibility
- ✓ Low molecular weight of the product



bach	Intrinsic viscosity	Molecular weight
1	1.03	197800
2	0.74	126000
3	0.71	119000
4	0.82	144900
5	0.81	142900
average	0.82	146120

Improvements for polymer reproducibility (test and errors):



- ✓ Vigorous stirring
- ✓ Strict thermal insulation
- ✓ High purity of monomers

Way to get more polymer



SCALED-UP 3-5 TIMES
ORIGINAL SYNTHESIS PROCESS: further scale ups were very difficult because both heat transfer and kinetics were controlling mechanisms due to the difficulty of obtaining a uniform temperature in the polymerization reactor

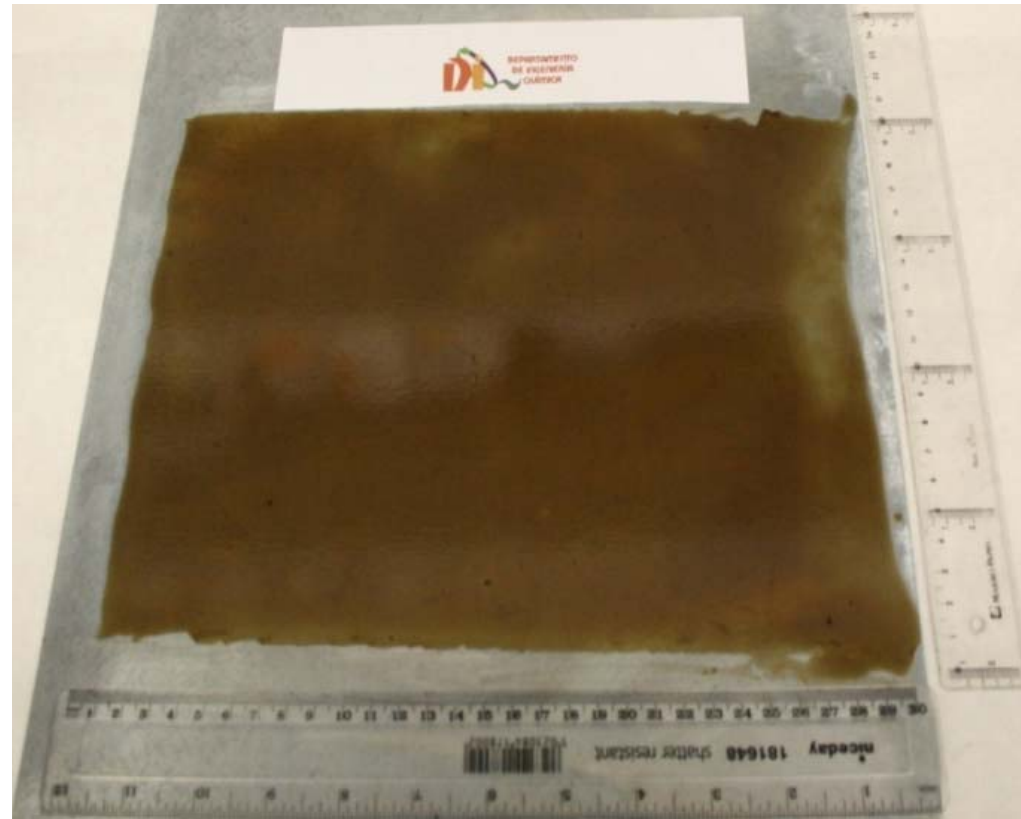
Batch number	Scale-up from the original process	Intrinsic viscosity (dl g ⁻¹)	PBI produced (g)
1	1:3	< 0.10	-
2	1:3	1.70	13.22
3	1:3	1.80	13.19
4	1:3	1.84	13.27
5	1:4	2.03	17.95
6	1:4	3.41	17.90
7	1:4	1.68	17.87
8	1:4	1.80	17.90
9	1:5	1.17	22.45

235 – 1013 kDa

Intermediate-high
molecular weight

Molecular weight
amplitude is acceptable
although not excessively
good (424 – 505 kDa)

Is it difficult to manufacture PBI membranes for HTPEMFC?



PBI membrane



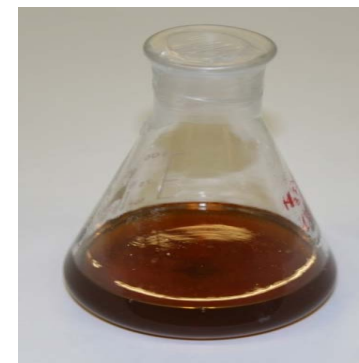
Membrane Casting



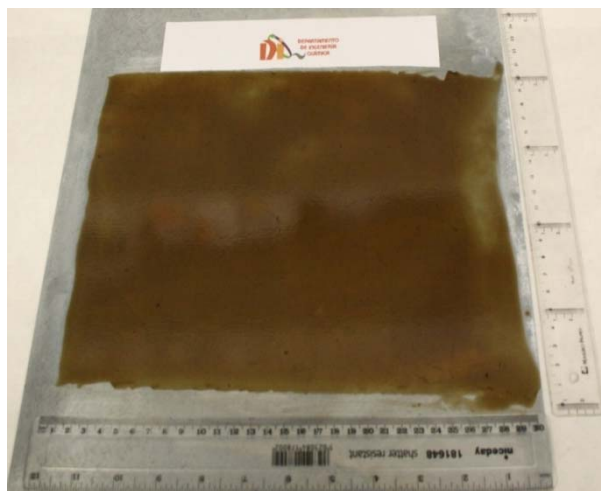
PBI powder

Dissolution in N,N'-
dimethylacetamide at 5% wt.

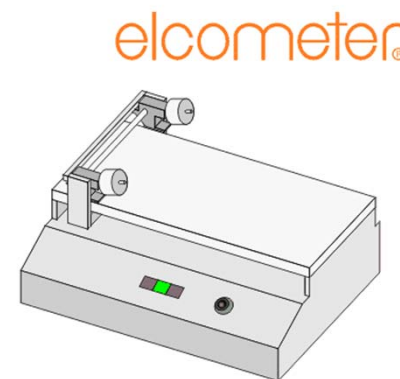
Vigorous stirring / 80-100 °C



PBI solution



PBI membrane



Elcometer 4330 / 4340 Motorised Film Applicator

Temperature ramp to evaporate the solvent and
immersion in water → peeling-off the plate &
washing

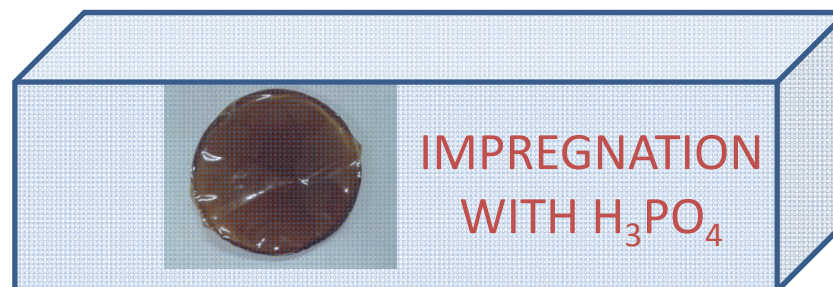
Key facts:



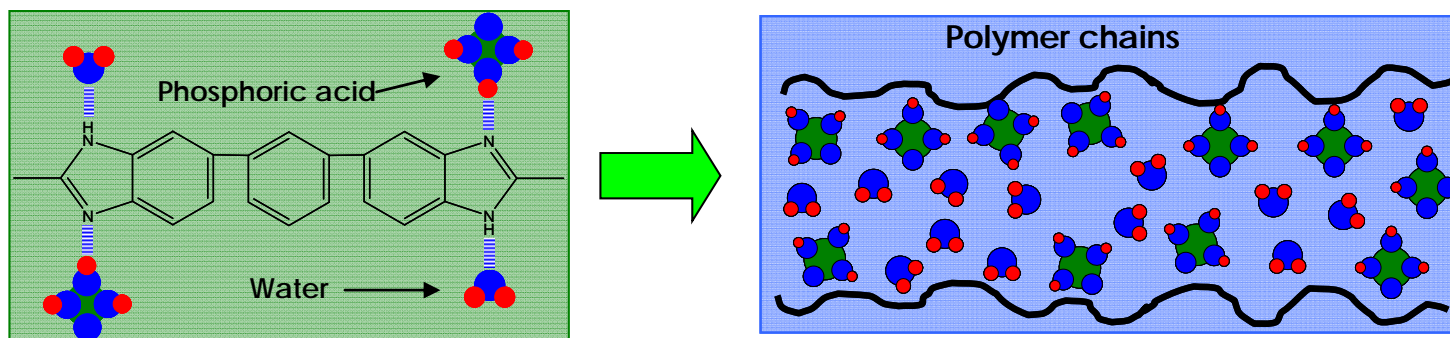
- Not difficult to obtain membranes up to 30 x20 cm² (DIN A4 size)
- A typical size for a membrane in a 5kW PEMFC stack could be around 200 cm² because larger areas lacks of:
 - ✓ Robustness (affecting lifetime)
 - ✓ uniform properties (affecting current distribution and, hence, efficiency)



Membrane impregnation



Phosphoric acid bath



❖ Chemical interaction between the polymer and the acid → 2 molecules per PBI repeating unit

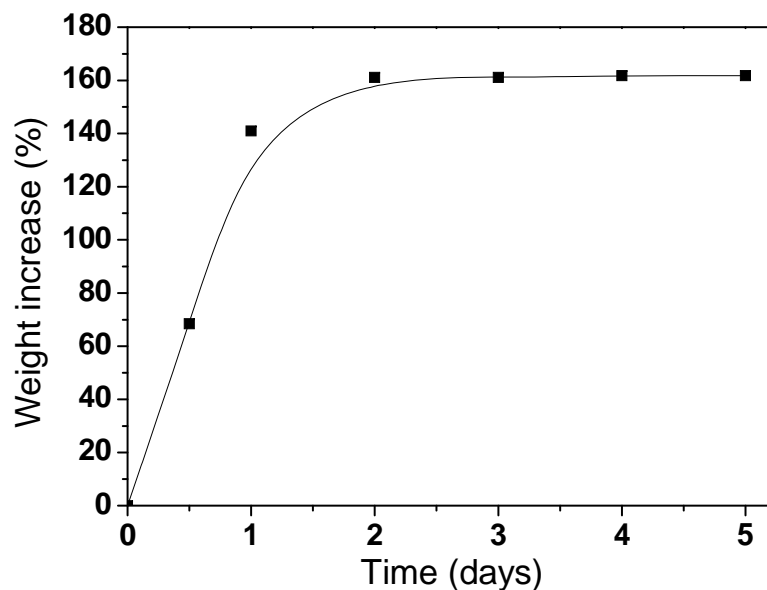
❖ More acid is placed between the polymer chains → swelling of the membrane

H ₃ PO ₄ bath solution (wt. %)	H ₃ PO ₄ uptake (mol · repeat unit PBI ⁻¹)	H ₂ O uptake (mol · repeat unit PBI ⁻¹)
75	5.3	5.9
85	11.3	11.6

High acid bath concentration

The higher the acid bath concentration, the higher the amount of absorbed acid per repeat unit of polymer

What about immersion time?



Time-course of the PBI membrane (thickness: 60 μm) weight increases over time after 85 wt. % H₃PO₄ solution bath immersion

Stationary value achieved
in 2 days of immersion

Ensure the entire
H₃PO₄ absorption



Membranes immersion
≥ 5 days in the acid bath

ACID LEACH

Phosphoric acid remained in PBI membranes after leaching and previously doped into different H_3PO_4 bath concentration solutions

Sample	H_3PO_4 bath solution (wt. %)	Remaining Acid (mol · repeat unit PBI^{-1})
PBI-5.3 mol H_3PO_4	75	0.62
PBI-11.3 mol H_3PO_4	85	0.89

$\approx 90\%$

Membranes lost most of the acid after being washed with hot water
 → The “free” H_3PO_4 absorbed by the membrane is softly linked to the polymer backbone

MECHANICAL STRENGHT

Mechanical properties of the PBI membranes at different doping levels. $T = 125\text{ }^\circ\text{C}$

Sample	Stress at break (MPa)	Elongation (%)
PBI	446.0	40.1
PBI-5.3 mol H_3PO_4	34.9	275.2
PBI-11.3 mol H_3PO_4	22.2	289.8

Membranes become softer and plastic when are doped

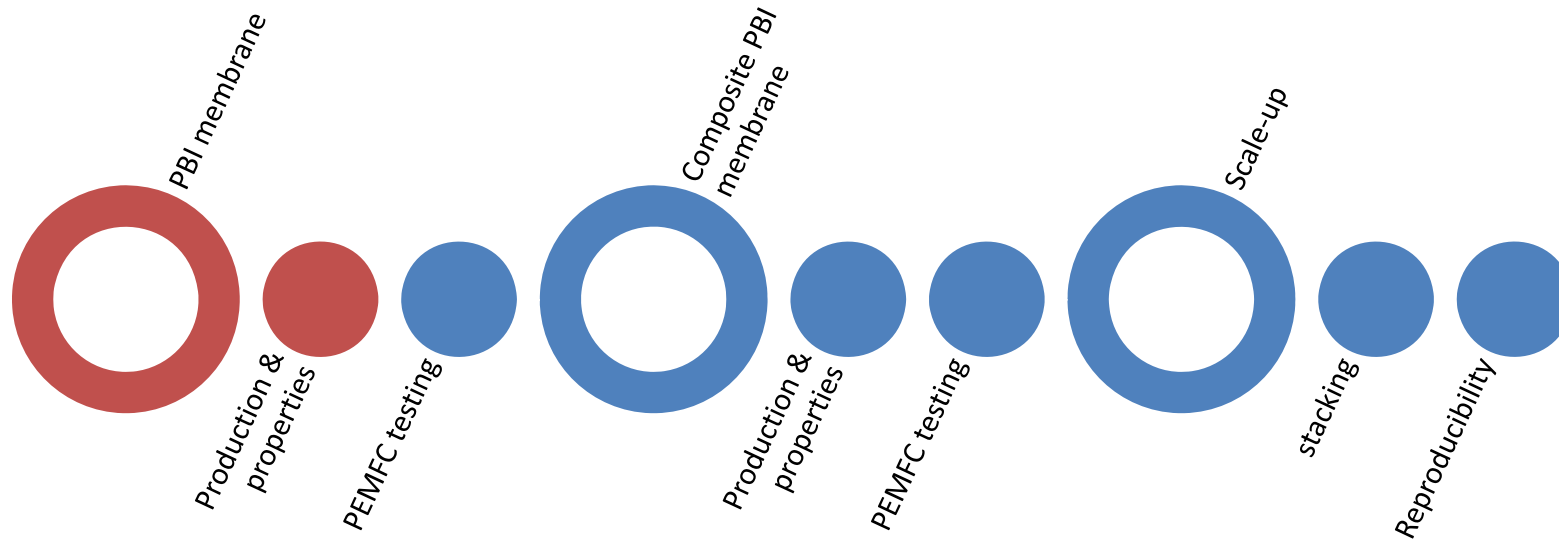
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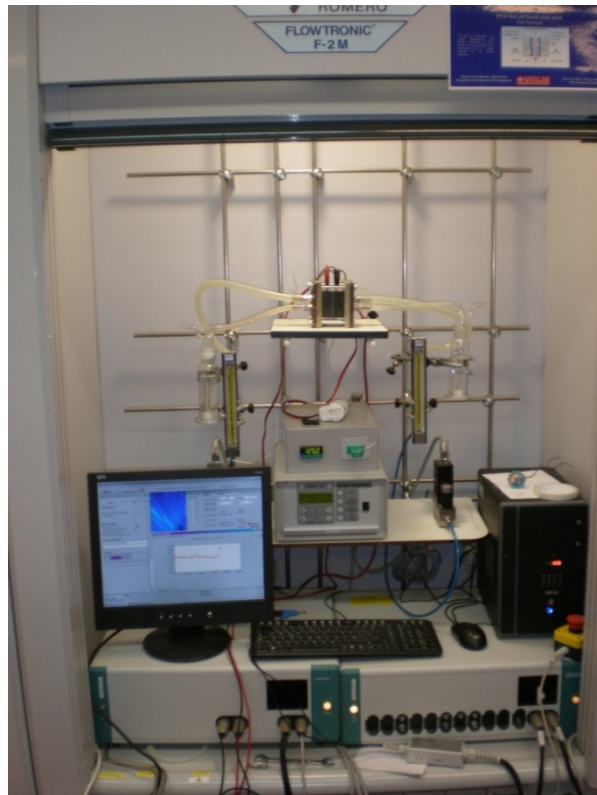
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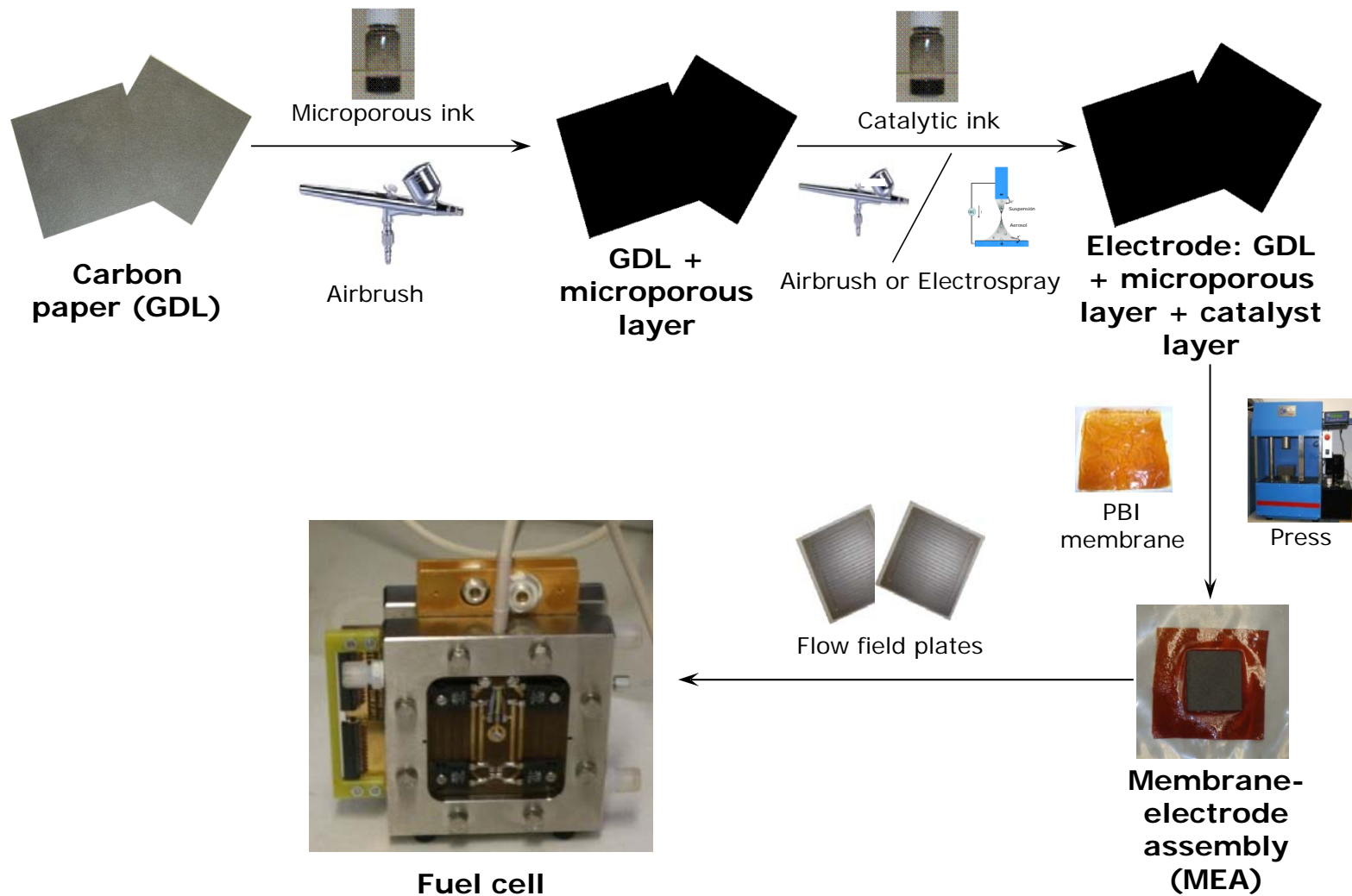


How do HTPEMFCs equipped with PBI membranes perform?



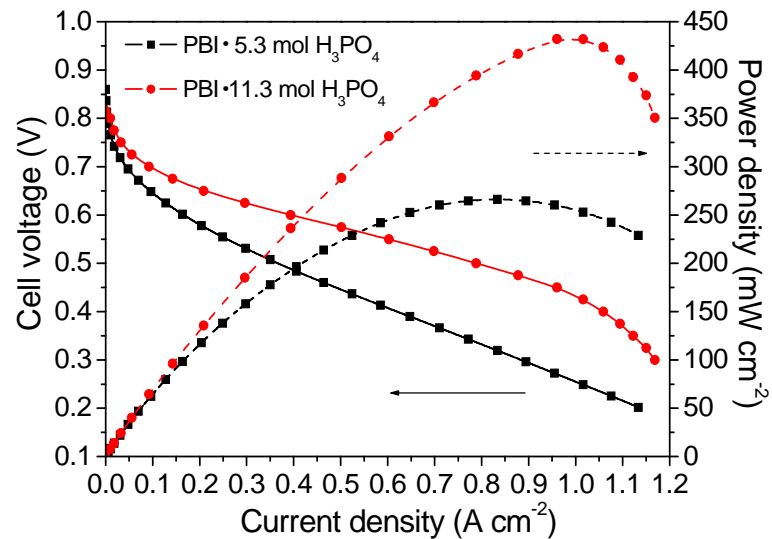


Preparation of MEAs

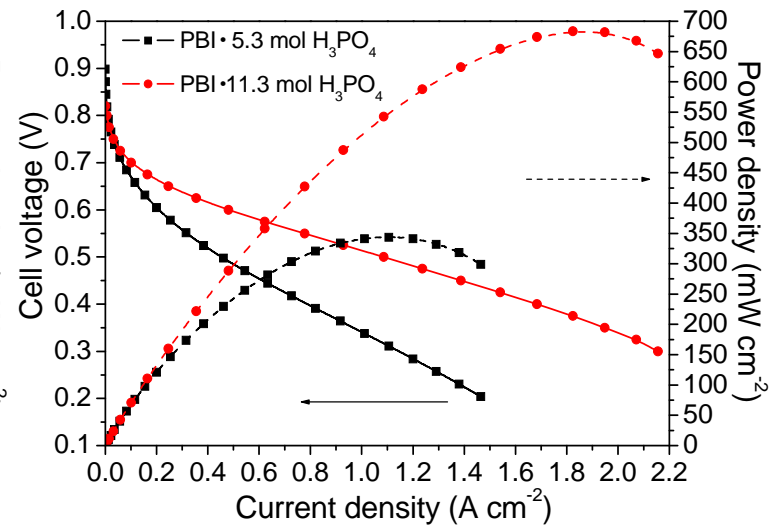




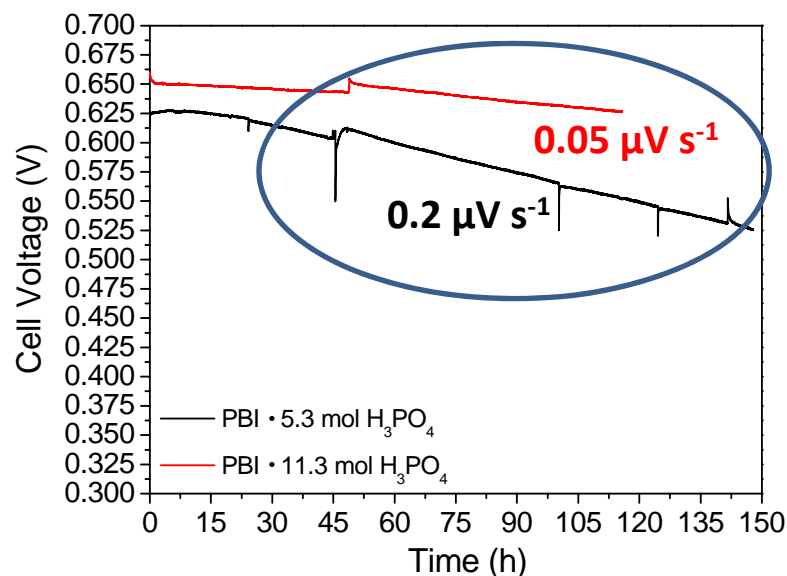
Fuel cell tests with PBI membranes



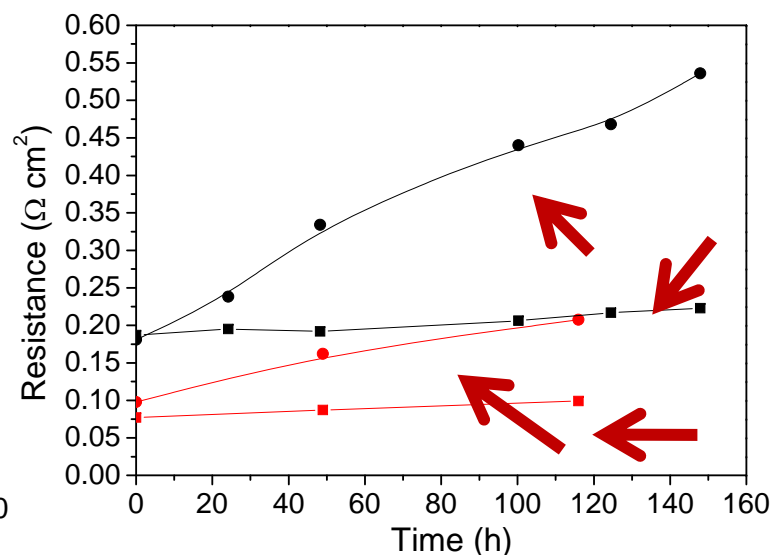
Polarization curves of PBI based fuel cells. $T = 125\text{ }^{\circ}\text{C}$



Polarization curves of PBI based fuel cells. $T = 175\text{ }^{\circ}\text{C}$



Fuel cell life test with PBI membranes impregnated into different acid bath concentrations studied in this Chapter. Voltage degradation versus time at 0.2 A cm^{-2} and $T = 175^\circ \text{C}$.



Ohmic (R_Ω , Squares) and charge transfer polarization ($R_{pol, ct}$, Circles) resistances variation for the different fuel cell in the life test. Black: PBI · 5.3 mol H_3PO_4 ; Red: PBI · 11.3 mol H_3PO_4

Irreversible voltage degradation

↑ PBI · 5.3 mol $\text{H}_3\text{PO}_4 \rightarrow$ PBI · 11.3 mol H_3PO_4

↑ Acid loss



Sample	$R_\Omega \text{ (m}\Omega \text{ cm}^2 \text{ h}^{-1})$	$R_{pol, ct} \text{ (m}\Omega \text{ cm}^2 \text{ h}^{-1})$
PBI · 5.3 mol H_3PO_4	0.23 ($r^2 = 0.941$)	2.34 ($r^2 = 0.984$)
PBI · 11.3 mol H_3PO_4	0.19 ($r^2 = 0.999$)	0.93 ($r^2 = 0.964$)

Low acid content \rightarrow Acid / Electrolyte loss is more noticeable along time



Worse kinetic for the reactions

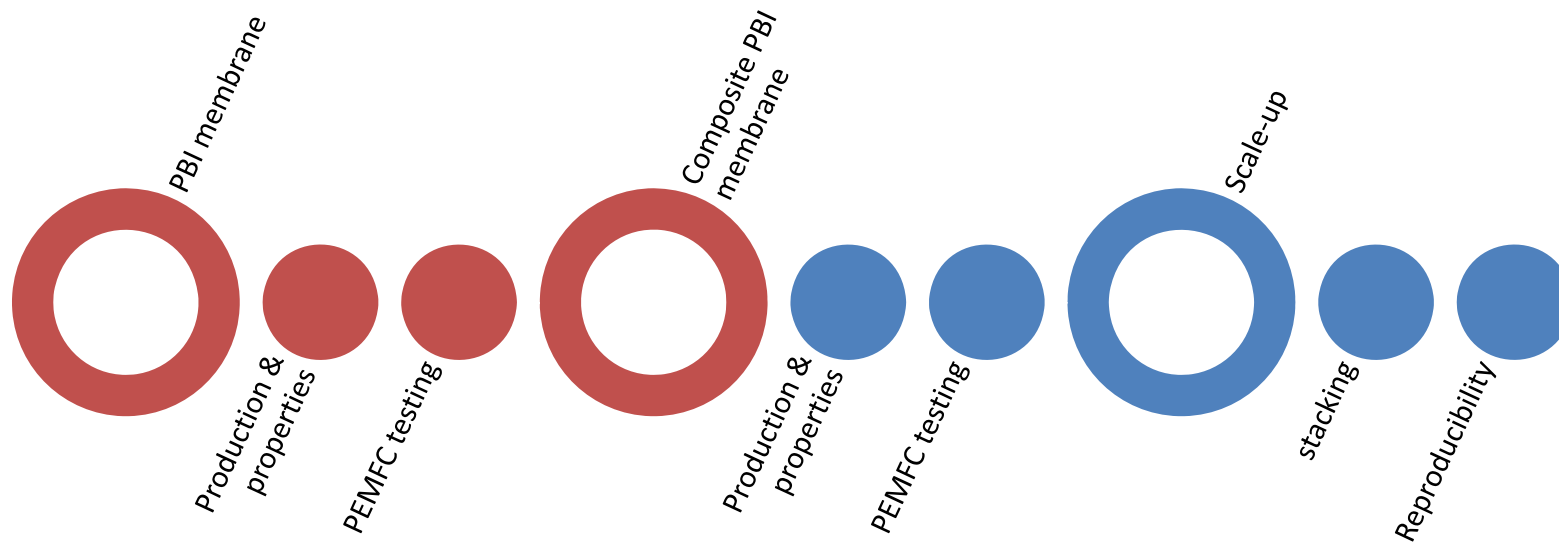
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Can we do something to increase service life and/or improve performance?



Inorganic fillers



▪ $\text{TiO}_2 \rightarrow$

Amphoteric and hydrophilic character:

- ✓ increase the acid doping level of the membrane
- ✓ membrane acid-retention capability
- ✓ minimizing the acid loss during operation in the fuel cell

▪ $\text{TiOSO}_4 \rightarrow$

Synergistic effect:

- ✓ filler is a TiO_2 precursor
- ✓ contains sulfates



Procedure to manufacture composite PBI membranes



PBI solution

+



TiO₂ / TiOSO₄

2, 4, 8 ó 16 % p/p

TiO₂ (anatase, d_m = 1,14 µm)

TiOSO₄ (≥ 29% Ti as TiO₂, d_m = 2,30 µm)

**Ultrasonicated
2 h**

**Mecanized
T = 80 °C
t = 8 h**

**Washing with
water**



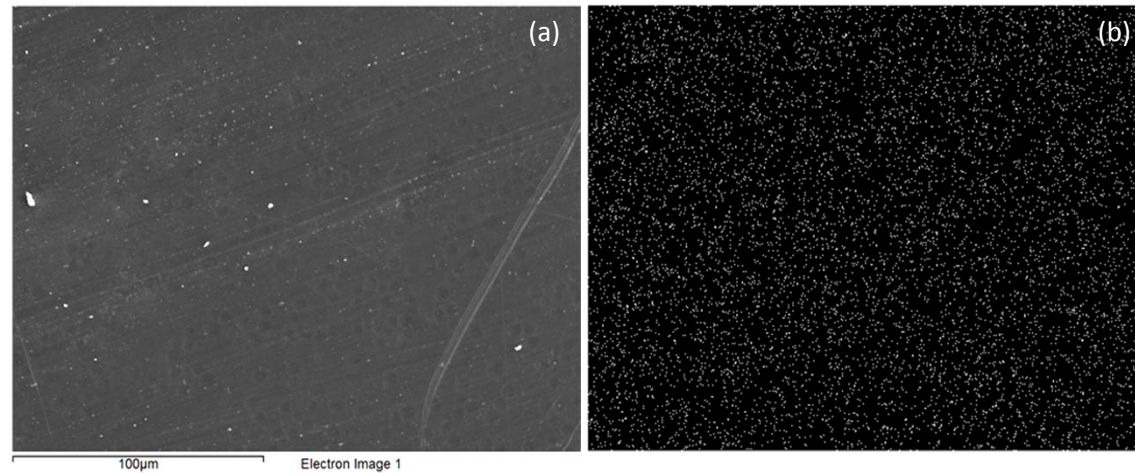
(a)

(b)

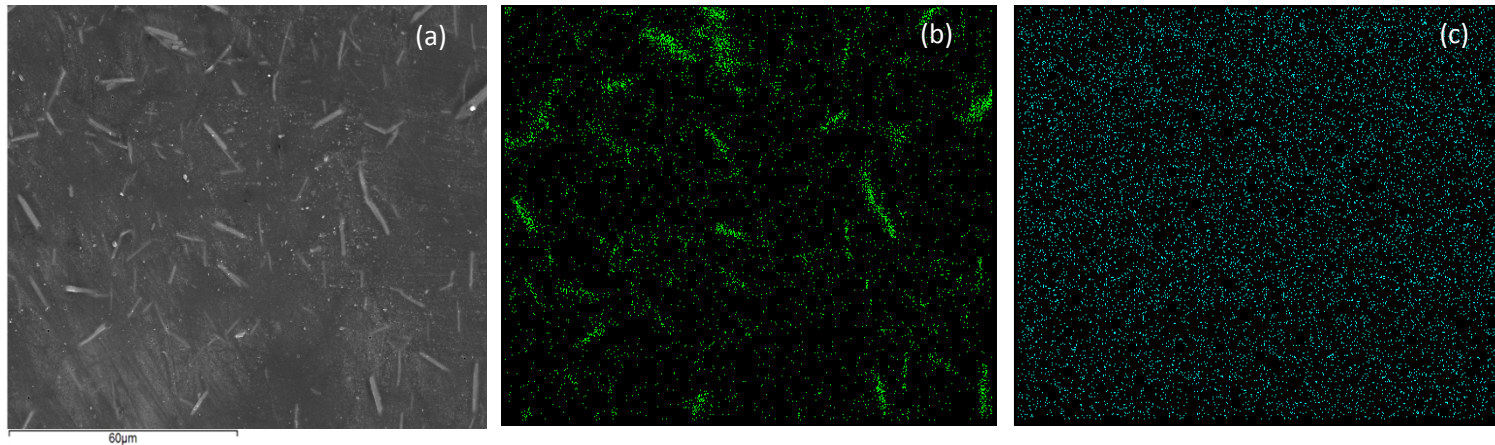
(c)

Pics of membranes obtained after mechanical process. (a) PBI Standart membrane; (b) PBI membrane with 16 % p/p TiO₂; (c) Pbi membrane with 16 % p/p TiOSO₄

SEM Y EDS



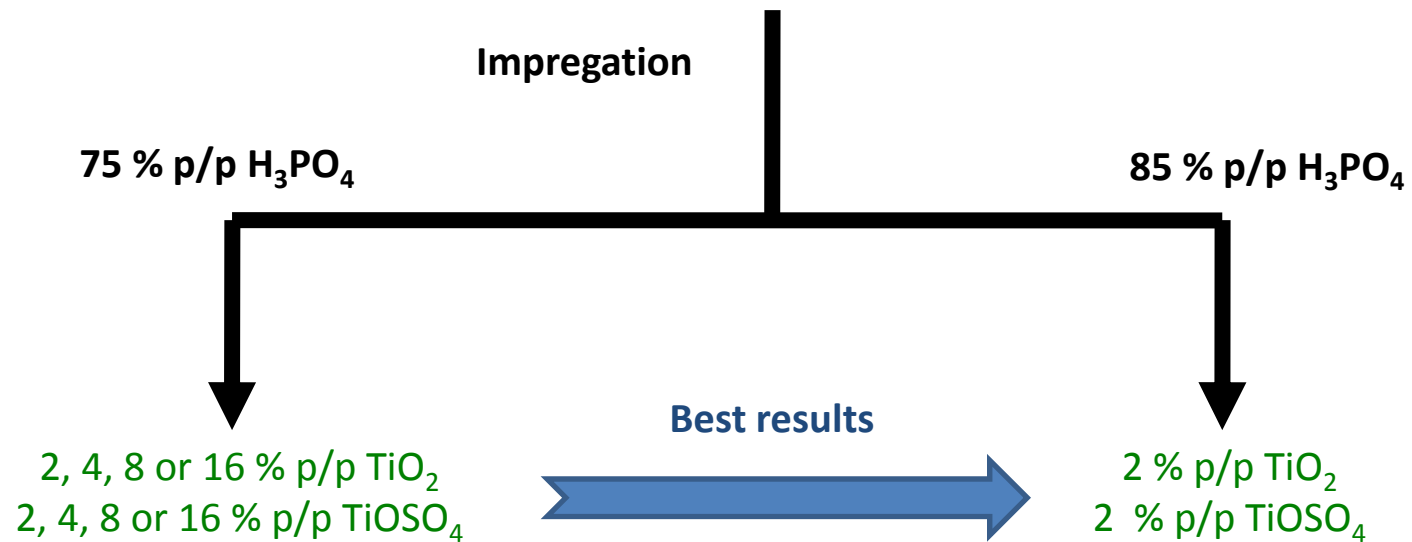
SEM micrographs of 2 % p/p en TiO_2 composite membrane surface (a) and distribution of titanium (b) in the membrane, obtained by mapping with EDS

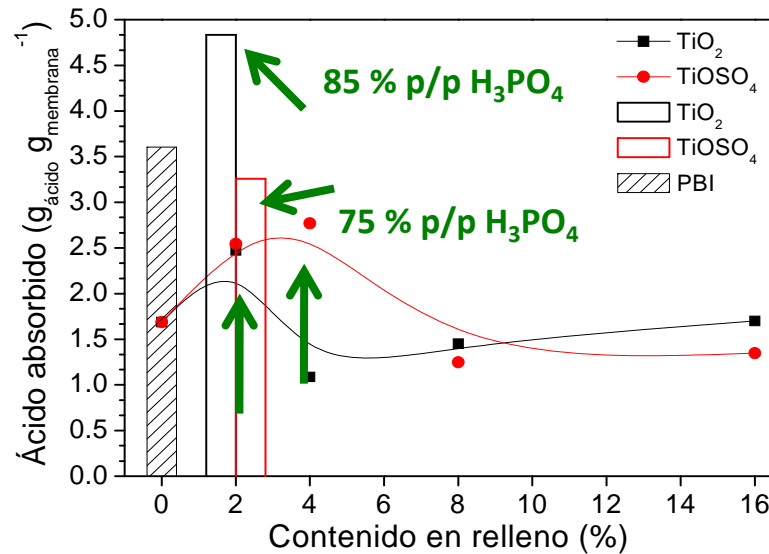


SEM micrographs of 2 % p/p TiOSO_4 composite membrane surface (a) and distribution of titanium (b) and sulfur (c) in the membrane, obtained by mapping with EDS

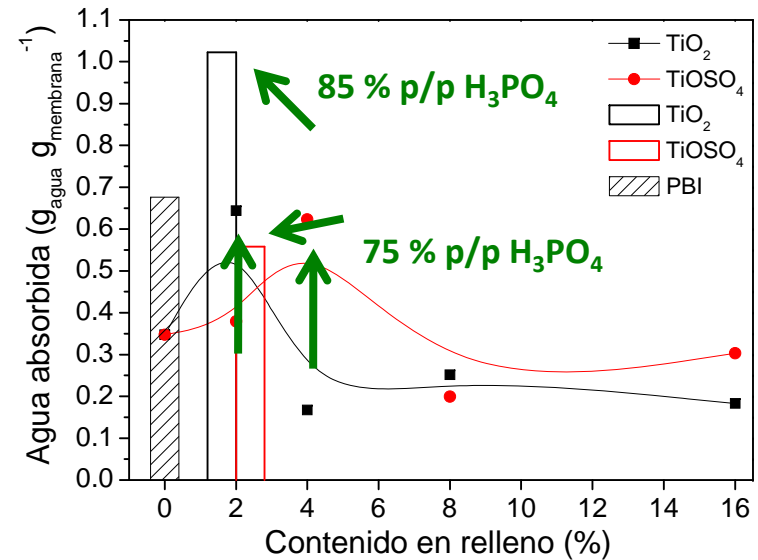


Composite PBI Membrane impregnation





Acid absorbed by different composite and standart PBI.
Lines: membranes doped into 75 % p/p H₃PO₄ solution.
Columns: membranes doped into 85 % p/p H₃PO₄ solution.



Water absorbed by different composite and standart PBI.
Lines: membranes doped into 75 % p/p H₃PO₄ solution.
Columns: membranes doped into 85 % p/p H₃PO₄ solution.

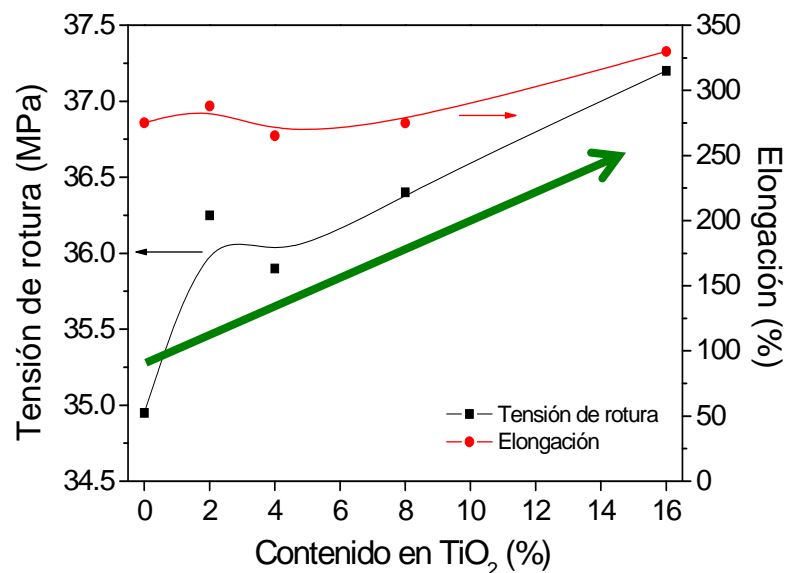
✓ 2 % p/p TiO₂ or 4 % p/p de TiOSO₄ into the polymer matrix were enough to retain higher amounts of acid and water than PBI.

✓ ↑ Filler concentration → Agglomerate formation →
→ ↓ active surface for acid and water absorption by the fillers

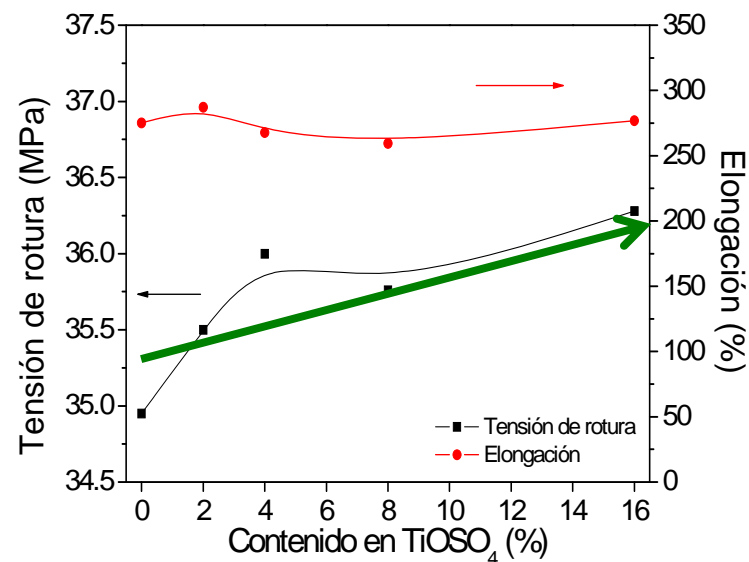
✓ TiO₂ membrane → ↑ Acid concentration → ↑ Doping level

✓ TiOSO₄ membrane → ↑ Acid concentration → ≈ Doping level

Mechanical stress



Breaking stress and γ elongation for composite PBI membranes with TiO_2 and standart. Impregnation bath: 75 % p/p H_3PO_4 . $T = 125^\circ\text{C}$



Breaking stress and γ elongation for composite PBI membranes with TiOSO_4 and standart. Impregnation bath: 75 % p/p H_3PO_4 . $T = 125^\circ\text{C}$

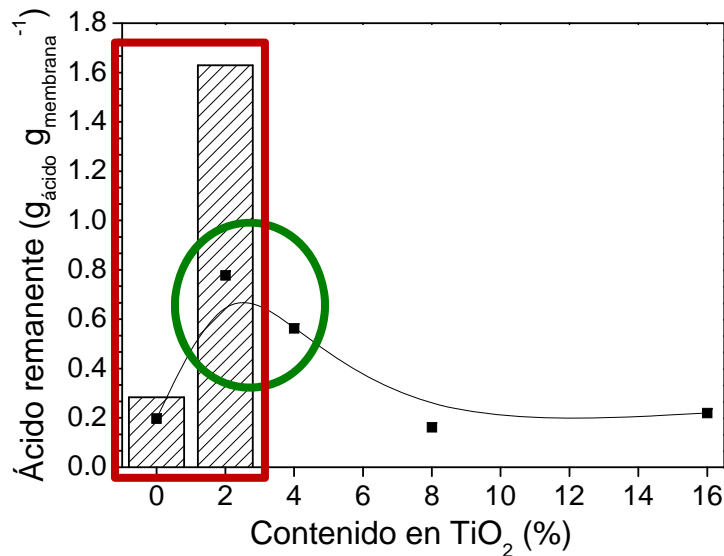
↑ x % $\text{TiO}_2 / \text{TiOSO}_4$



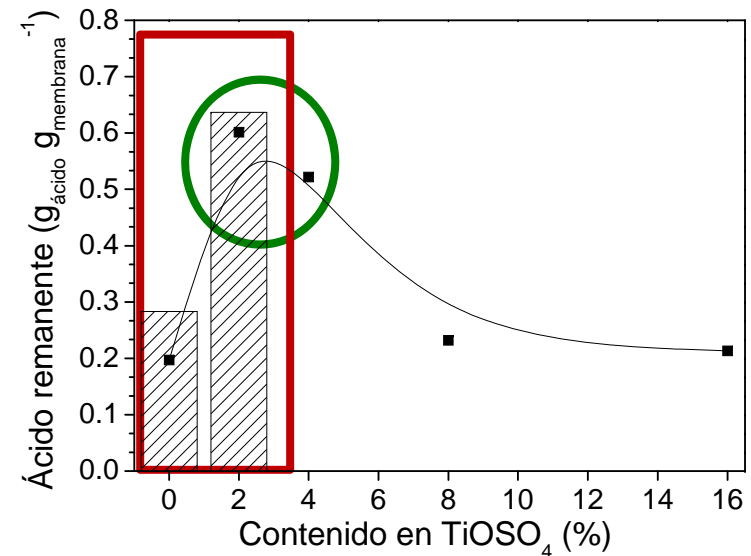
↑ Breaking stress
↑ Elongation

✓ ↓ Weakness for composite membranes due to the inorganic reinforcing presence.

ACID LEACH



Phosphoric acid retained by TiO_2 composite membranes after lixiviation process. Lines: membranes doped with 75 % p/p H_3PO_4 solution. Columns: membranes doped with 85 % p/p H_3PO_4 solution.



Phosphoric acid retained by TiOSO_4 composite membranes after lixiviation process. Lines: membranes doped with 75 % p/p H_3PO_4 solution. Columns: membranes doped with 85 % p/p H_3PO_4 solution.

2 y 4 % TiO_2 / TiOSO_4

Impregnated with $[\text{H}_3\text{PO}_4] = 75$ % p/p

2 % TiO_2 / TiOSO_4

Impregnated with $[\text{H}_3\text{PO}_4] = 85$ % p/p



↑ Higher capability retention



**2 % TiO_2 -PBI → Higher capability retention
+ 5 times lesser than standart PBI**

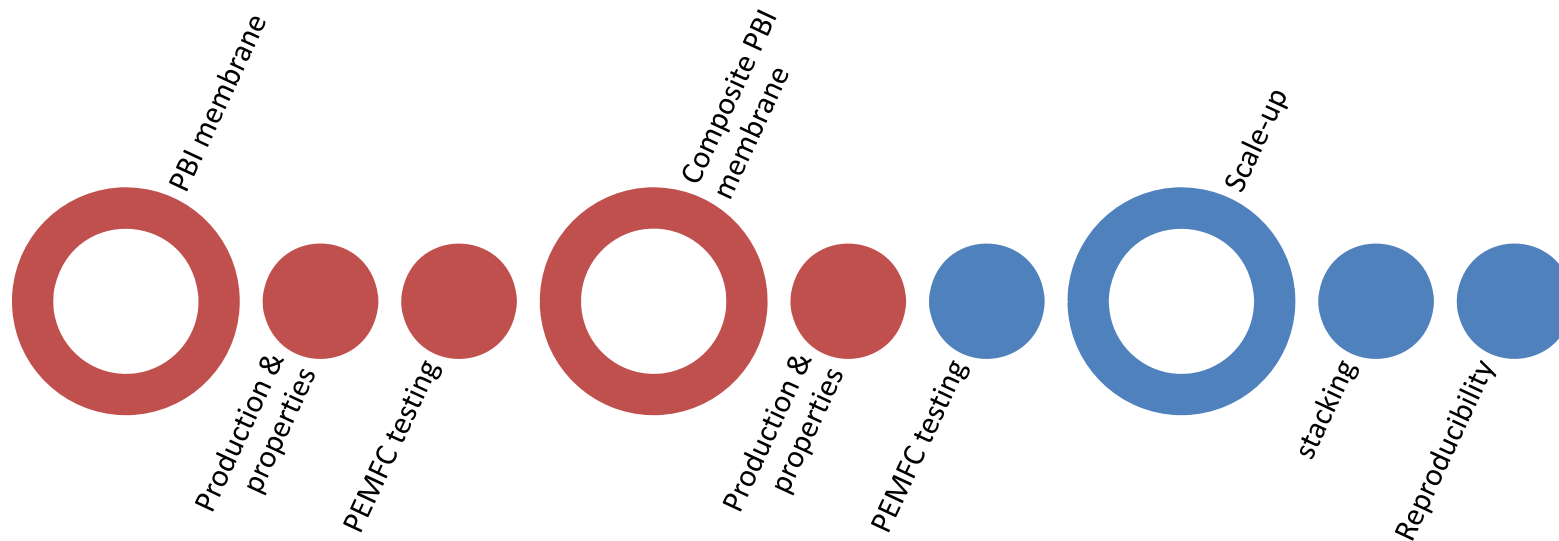
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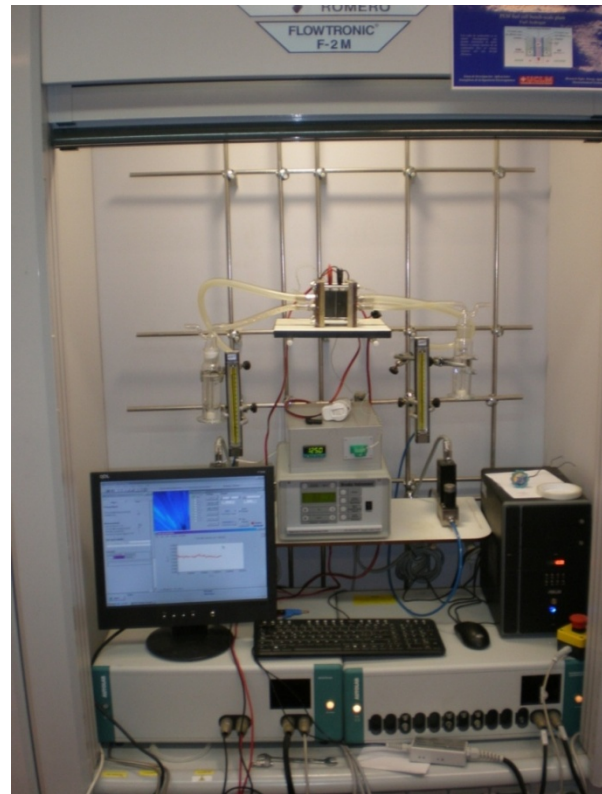
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How do HTPeMFCs equipped with composite PBI membranes perform?





Fuel cell tests with composite PBI membranes

Membranes which were expected to have better performances in HTPeMFC

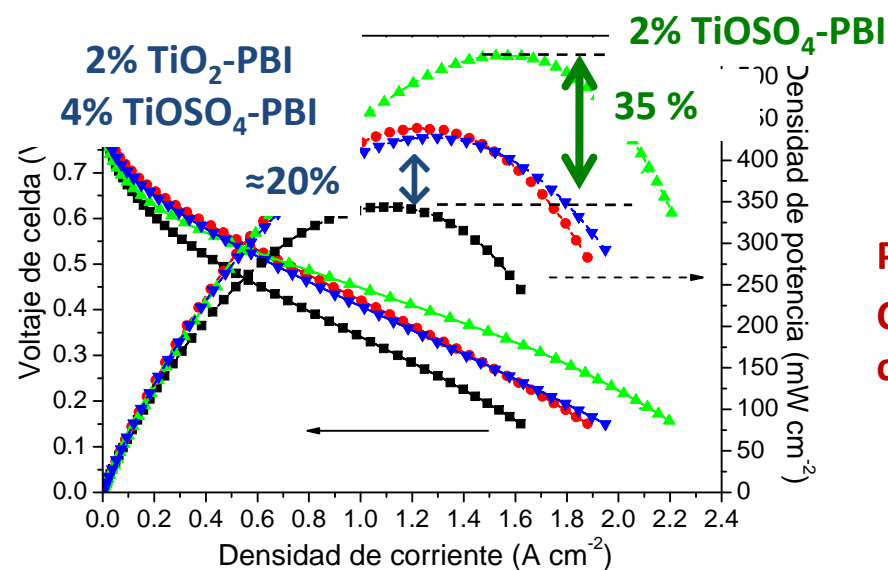


2 % TiO_2 -PBI



2 y 4 % TiOSO_4 -PBI

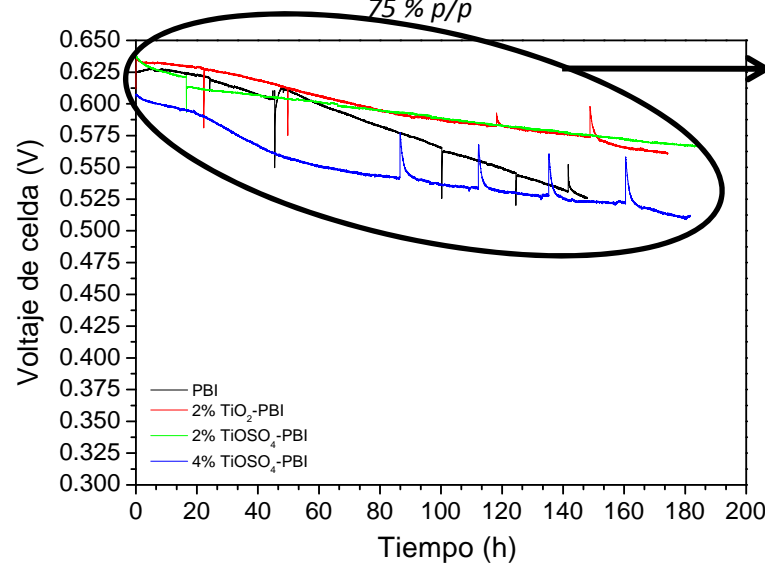
- ✓ larger acid and water absorption .
- ✓ higher acid retention capabilities .
- ✓ highest ionic conductivities.



Membrane doped with
75 % p/p H_3PO_4

Performance:
Composite PBI cells > standard PBI cells

Polarization curves for fuel cells with Standard PBI and TiO_2 y $TiOSO_4$ composite membranes. $T = 175^\circ C$. $[H_3PO_4] = 75\% \text{ p/p}$



PBI: $0,2 \mu V s^{-1}$

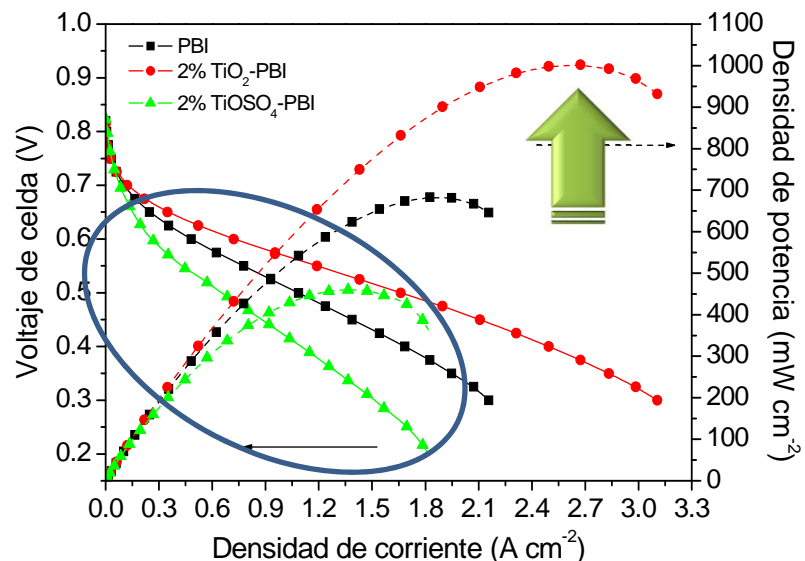
2% TiO_2 -PBI: $0,12 \mu V s^{-1}$

2% $TiOSO_4$ -PBI: $0,09 \mu V s^{-1}$

4% $TiOSO_4$ -PBI: $0,13 \mu V s^{-1}$

Life test carried out for fuel cells operating with the different membranes. Voltage vs time at $0.2 A cm^{-2}$, $T = 175^\circ C$. $[H_3PO_4] = 75\% \text{ p/p}$

Sample	R_Ω ($m\Omega cm^2 h^{-1}$)	$R_{pol, ct}$ ($m\Omega cm^2 h^{-1}$)
PBI	0,23 ($r^2 = 0.941$)	2,34 ($r^2 = 0.984$)
2 % TiO_2 -PBI	0,09 ($r^2 = 0.939$)	1,17 ($r^2 = 0.844$)
2 % $TiOSO_4$ -PBI	0,11 ($r^2 = 0.978$)	0,26 ($r^2 = 0.670$)
4 % $TiOSO_4$ -PBI	0,19 ($r^2 = 0.990$)	2,40 ($r^2 = 0.860$)



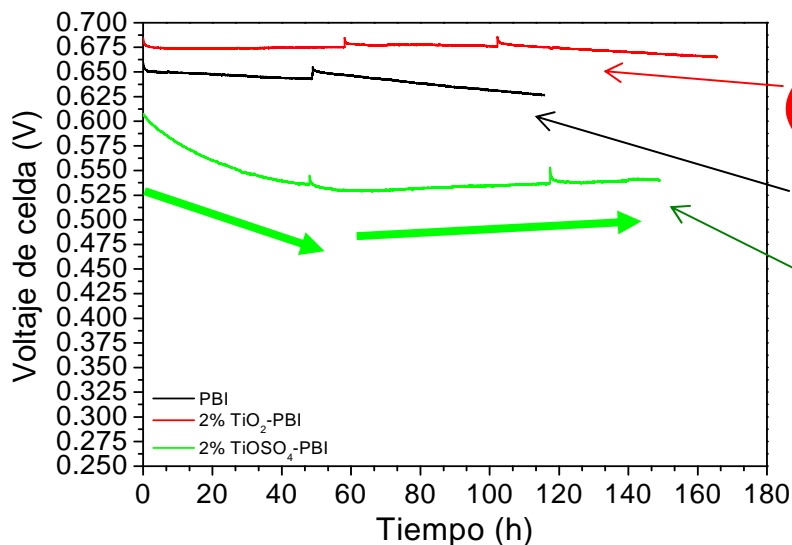
Polarization curves for fuel cells with standart PBI and composite TiO_2 and TiOSO_4 membranes. $T = 175^\circ\text{C}$.
 $[\text{H}_3\text{PO}_4] = 85\% \text{ p/p}$

Membrane doped with
 85 % p/p H_3PO_4

Worst performance: 2% TiOSO_4 -PBI

Best performance: 2% TiO_2 -PBI

1 W cm^{-2}



Life test carried by fuel cells operating with the different membranes. Cell voltage vs time 0.2 A cm^{-2} , $T = 175^\circ\text{C}$.
 $[\text{H}_3\text{PO}_4] = 85\% \text{ p/p}$

0.01 $\mu\text{V s}^{-1}$

0.05 $\mu\text{V s}^{-1}$

0.06 $\mu\text{V s}^{-1}$

Extrange behaviour:
 2% TiOSO_4 -PBI

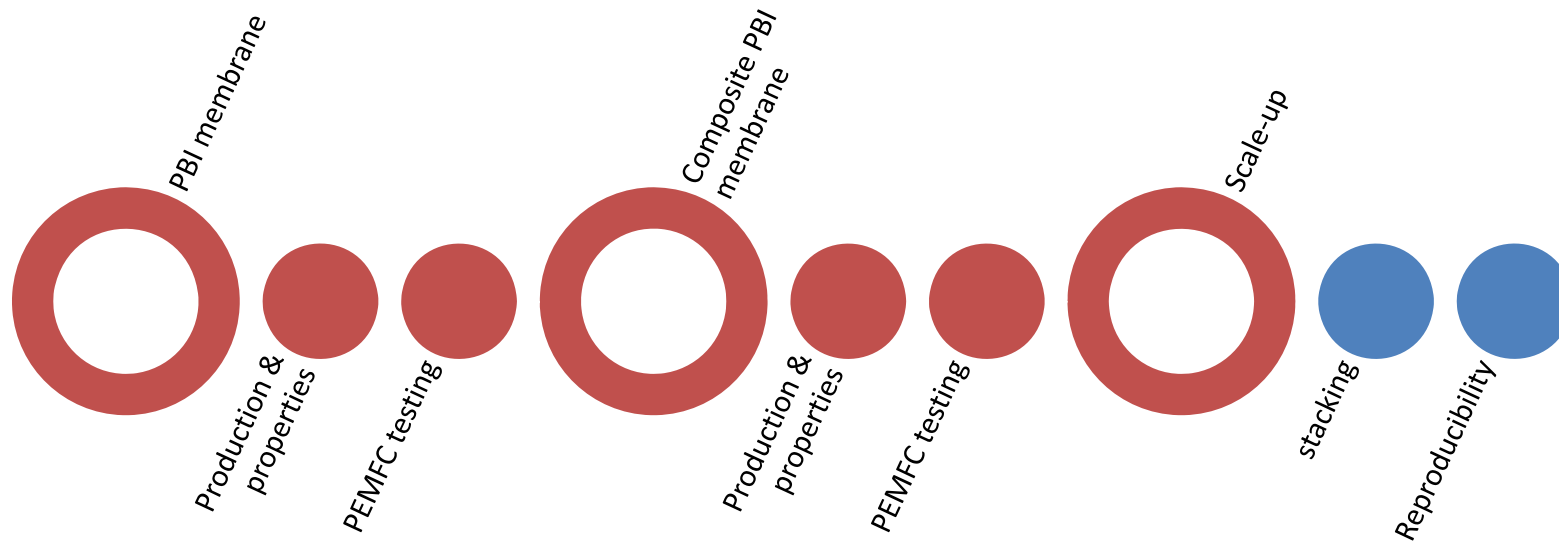
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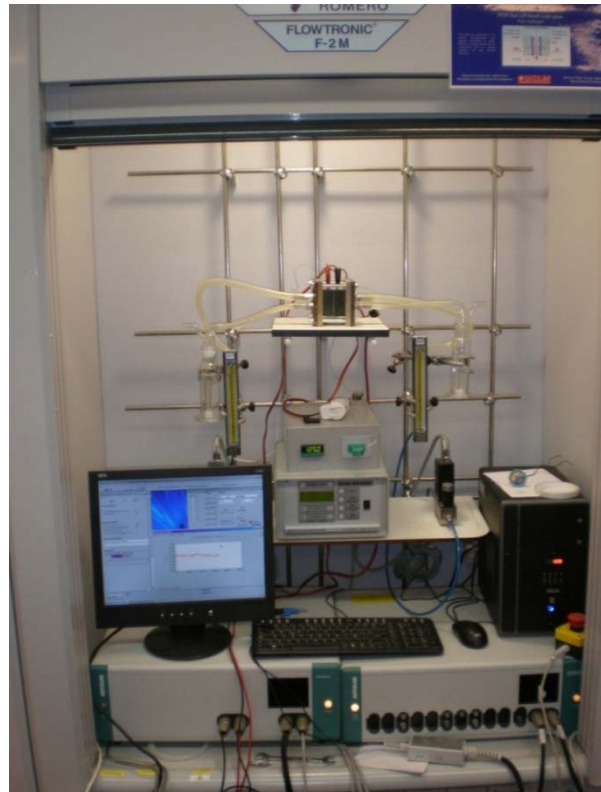
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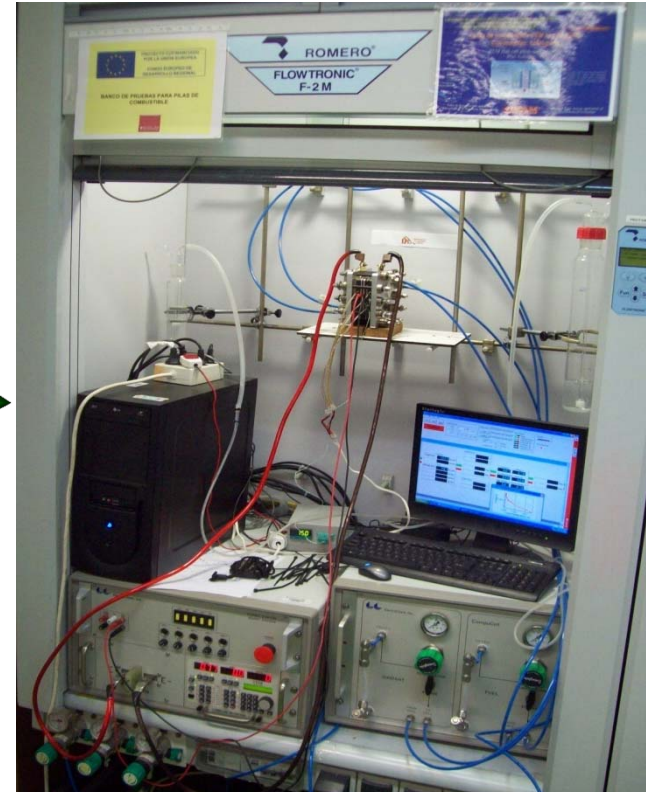
Evaluation of the current and composition distribution to check for main causes of rapid decay



Does size matters?



POTENCIOSTAT/GALVANOSTAT
FOR FUEL CELL
CHARACTERIZATION(20 A)



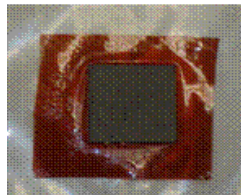
WORK STATION FOR FUEL CELL
CHARACTERIZATION (150 A)



Scale up of HTPeMFC



1) Increase cell size



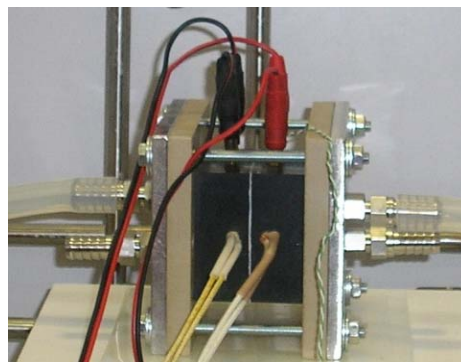
Area: 5 cm²



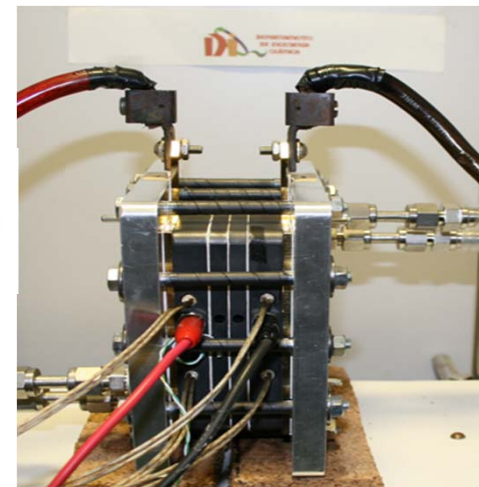
Area: 50 cm²



2) stacking



SINGLE CELL (1 MEA)



STACK (3 MEA)



Manufacturing of two fuel cell stacks



Fuel cell with doped PBI
membrane $[\text{H}_3\text{PO}_4] = 75\% \text{ p/p}$
(SFCS)

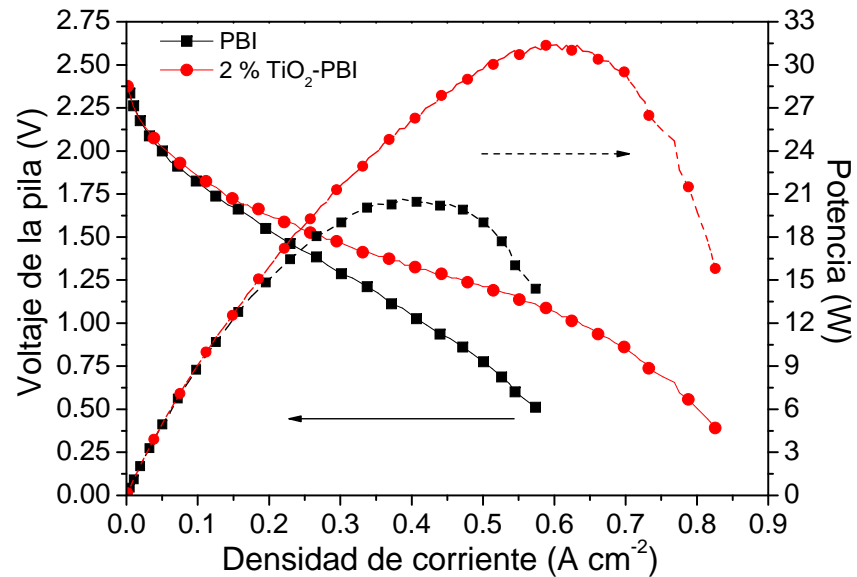
✓ Reference technology

Fuel cell with membrane 2 % TiO_2 -
PBI doped with $[\text{H}_3\text{PO}_4] = 85\% \text{ p/p}$
(CFCS)

- ✓ Acid Absorption (+ adsorption)
- ✓ Acid retention
- ✓ Proton conductivity
- ✓ Performance in a fuel cell
- ✓ Stability in a fuel cell

- ✓ 3 cells
- ✓ $50 \text{ cm}^2 / \text{Cell}$
- ✓ total: 150 cm^2

Performance of stack



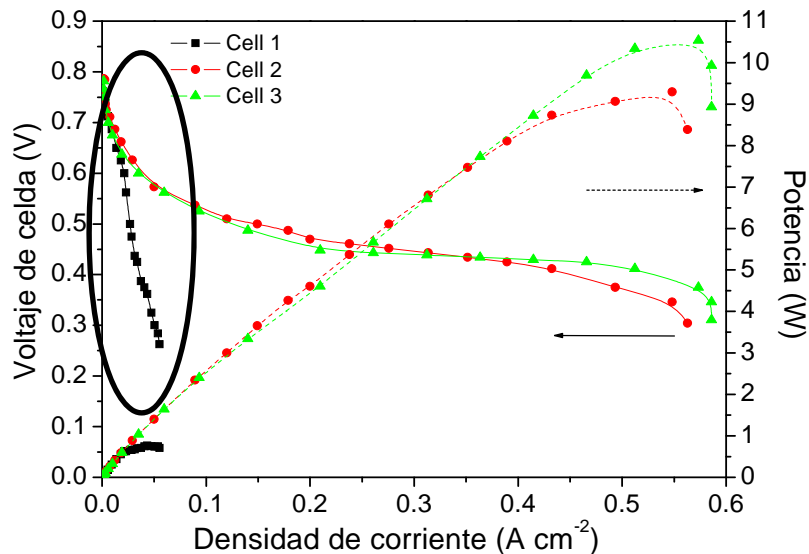
Polarization curves of SFCS and CFCS. $\lambda_{\text{H}_2} = 2$, $\lambda_{\text{O}_2} = 3$; $T = 125$ °C; $P = 1$ atm

Previous test:

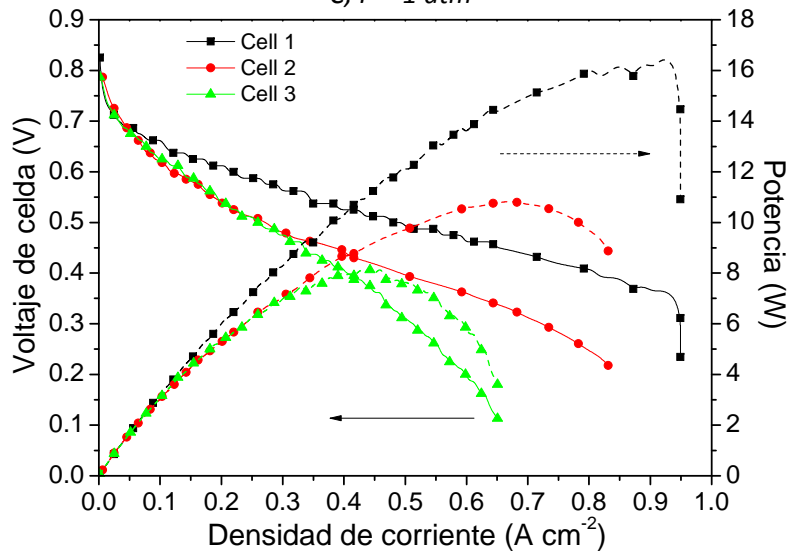
- 1) conditioning stage
- 2) shut-down stage

Best performance: HTPeMFC - 2% TiO_2 -PBI (CFCS)

Performance of cells inside the stack



Polarization curves of each cell SFCS. $\lambda_{H_2} = 2$, $\lambda_{O_2} = 3$; $T = 125$ °C; $P = 1$ atm



Polarization curves of each cell of CFCS. $\lambda_{H_2} = 2$, $\lambda_{O_2} = 3$; $T = 125$ °C; $P = 1$ atm

Different performance of cells in the stack



Low reproducibility for scale up

Cell 1 (SFCS) → worst performance

deactivation of the catalyst?

mechanical damage of the membranes?

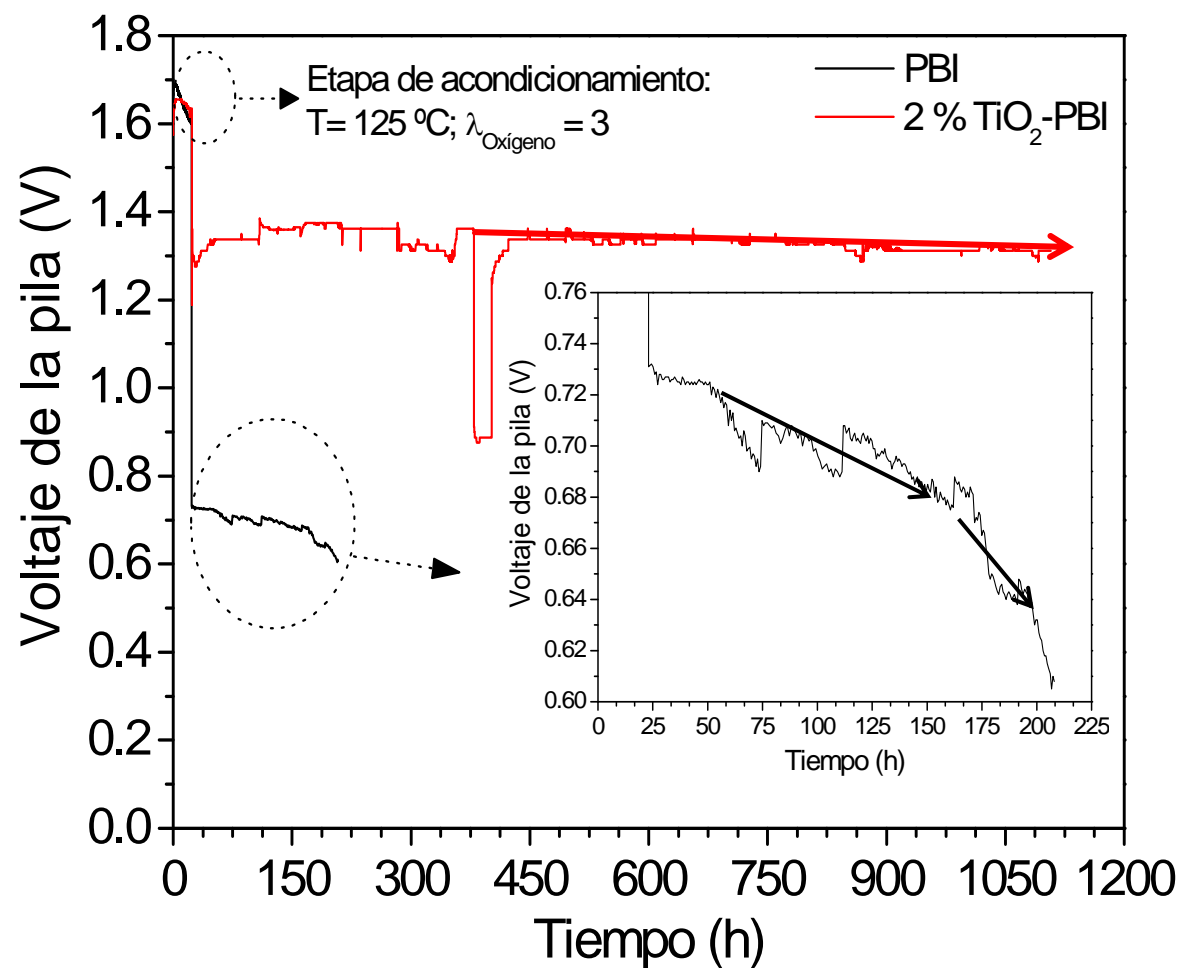


Where& When?:

- manufacturing of MEA
- assembling
- stacking
- conditioning

Lifetest

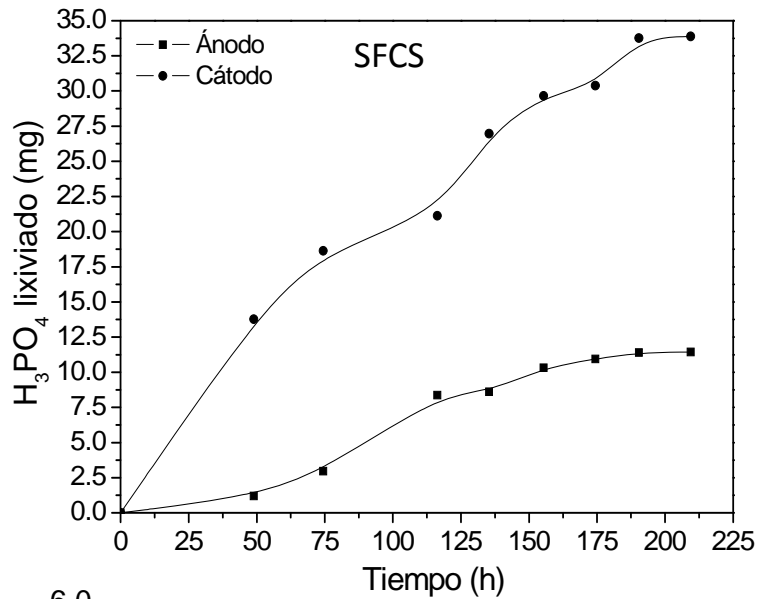
CFSF and SFCS operated at constant current density ($0,2 \text{ A cm}^{-2}$)



Performance decay < 2 % after 1100 h operation (total time: 1.700 h de estudio including testing and shut ups)

Voltage variation in life test (conditioning stage included). Current density= 0.2 A cm^{-2} ; $\lambda_{\text{H}_2} = 2$, $\lambda_{\text{Aire}} = 3$; $T = 150 \text{ °C}$; $P = 1 \text{ atm}$

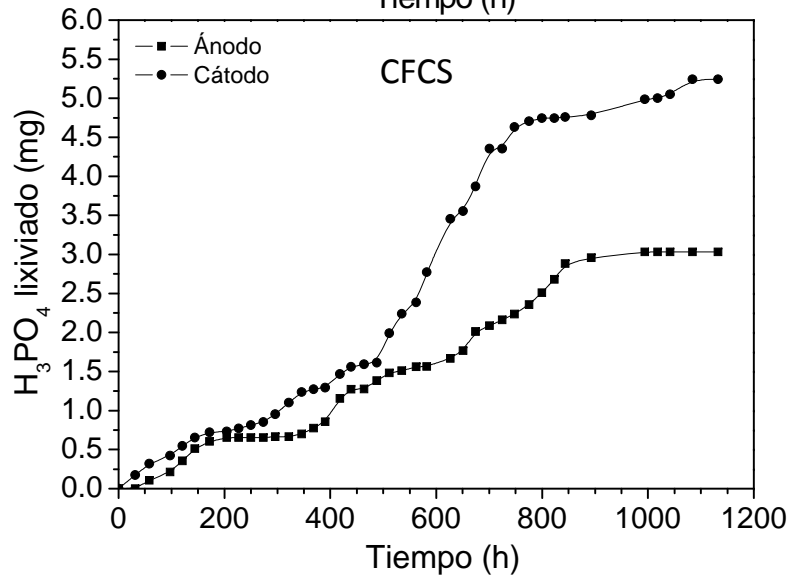
Acid leached during lifetest



❖ ↑ acid leach more from the cathode side than from the anode side → water vapour generated in the reaction on the cathode side dragged part of the phosphoric acid outside the fuel cells

❖ CFCS total acid leached < 0,6 %

❖ SFCS total acid leached = 2 %



H₃PO₄ lixiviated of anode and cathode for each fuel cell during the operation at constant load.

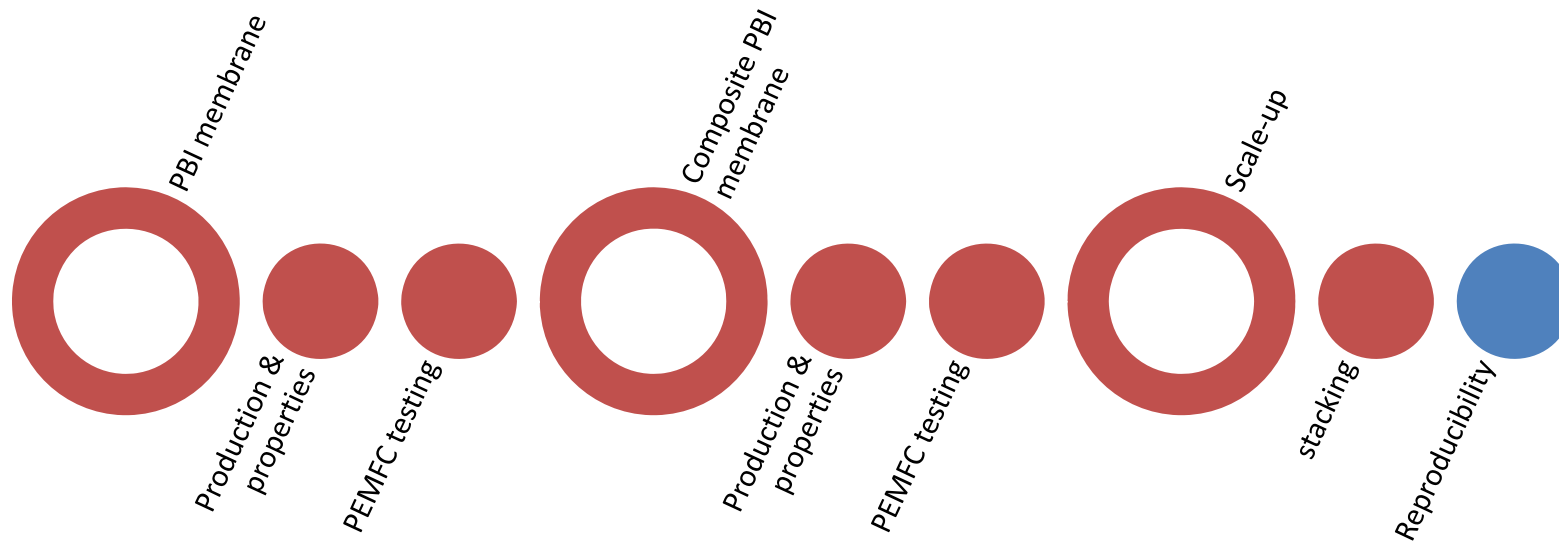
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Evaluation of the current and composition distribution to check for main causes of rapid decay



What's the matter with reproducibility?

deactivation of the catalyst?

mechanical damage of the
membranes?



Where & When?:

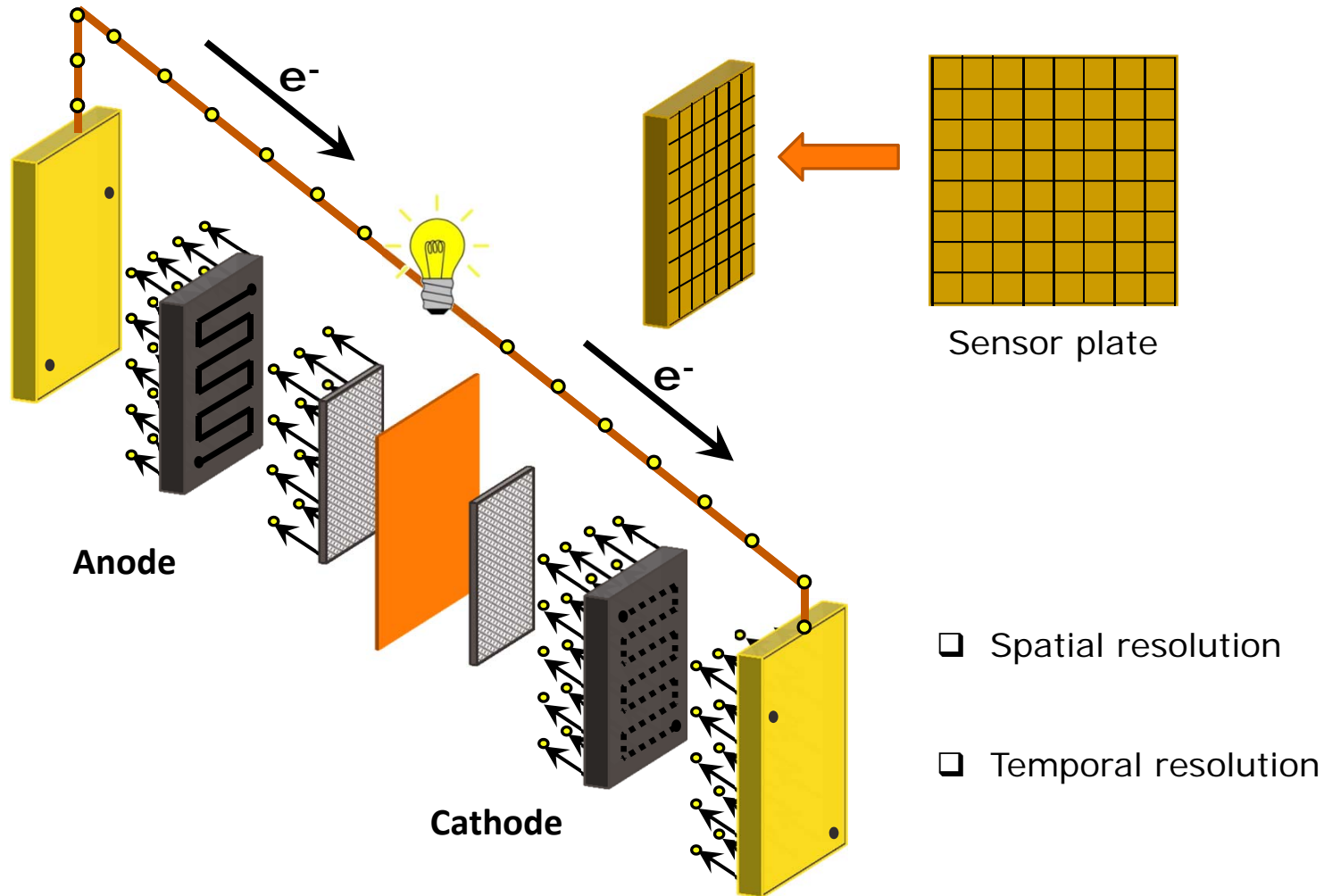
- manufacturing of MEA
- assembling
- stacking
- conditioning



How to get a uniform behaviour?

Could current distribution measurement help to
understand this low reproducibility?

➤ Apparatus – Placement of the measuring device



Lifetest I: airbrush; anode: 0.25 mg Pt cm⁻² ; cathode: 0.25 mg Pt cm⁻²

Lifetest II: electrospray; anode: 0.25 mg Pt cm⁻² ; cathode: 0.25 mg Pt cm⁻²

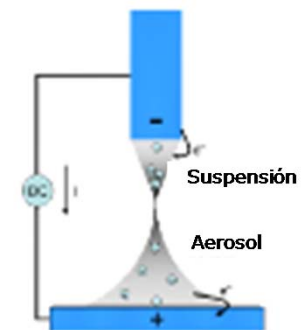
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Spread catalytic ink technique:



airbrush



electrospray

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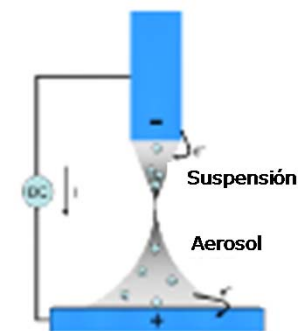
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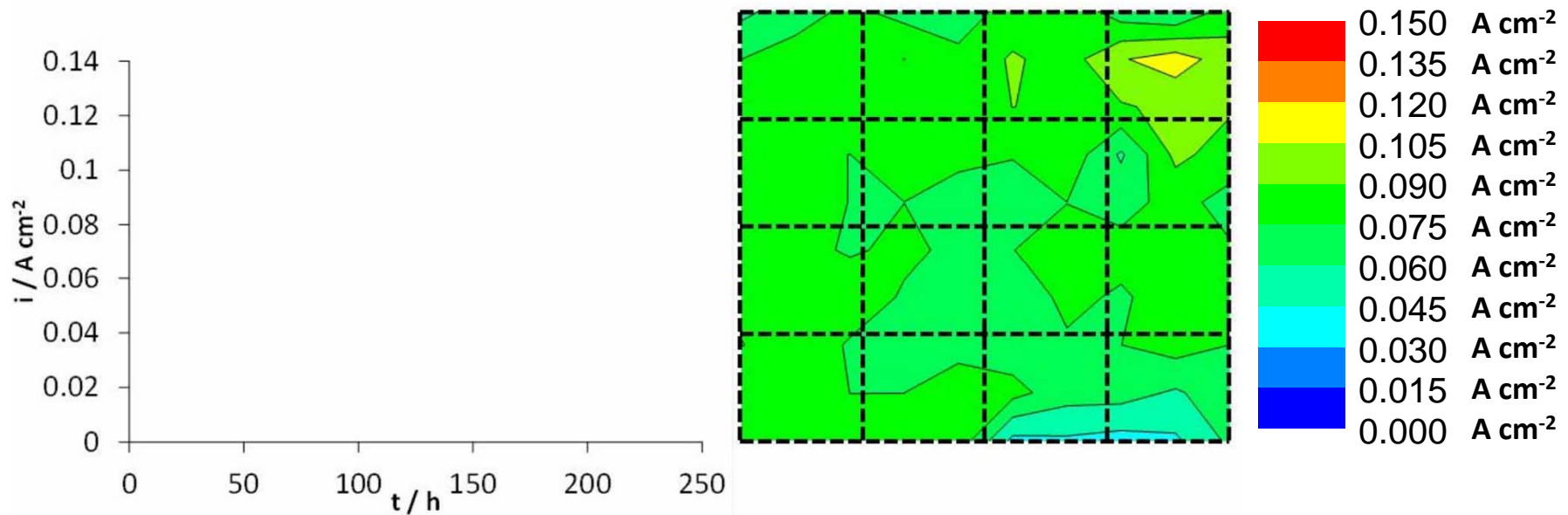
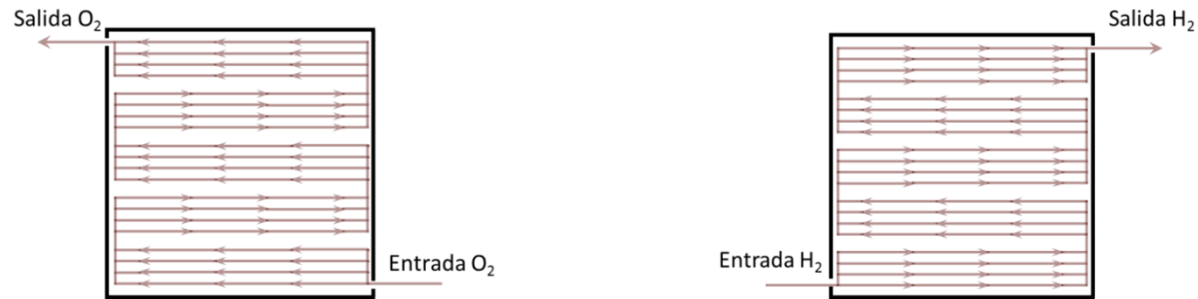
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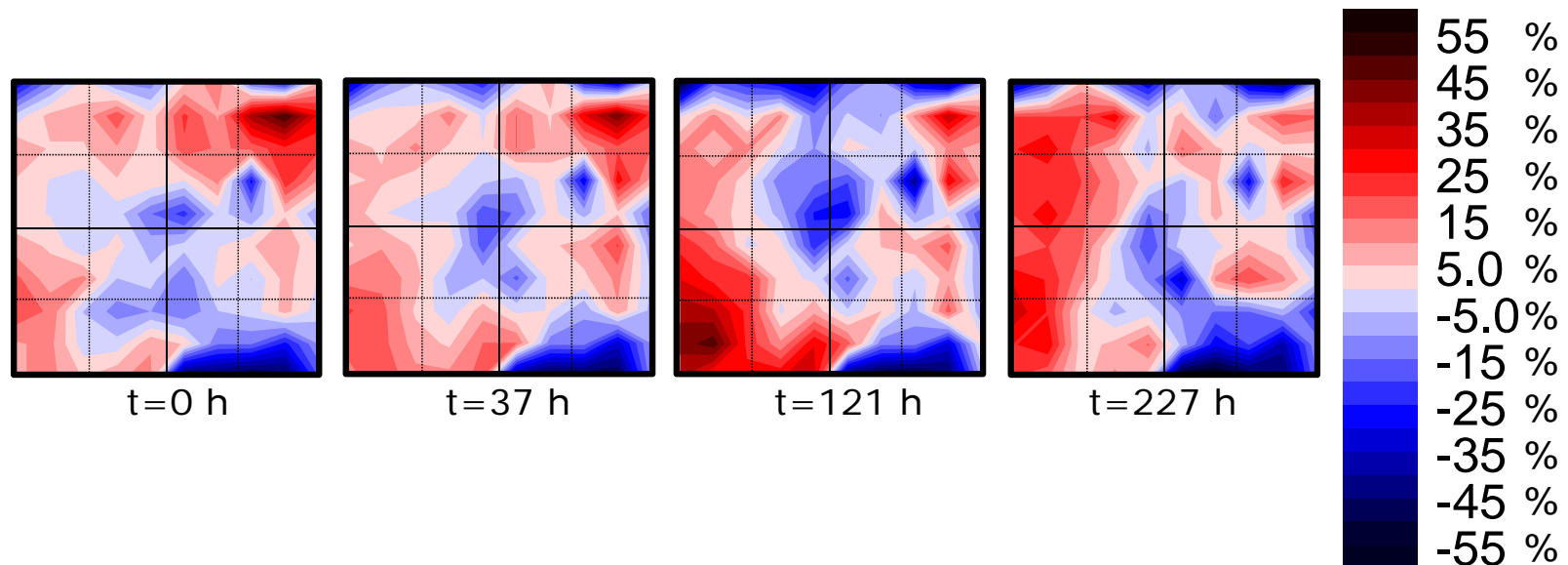
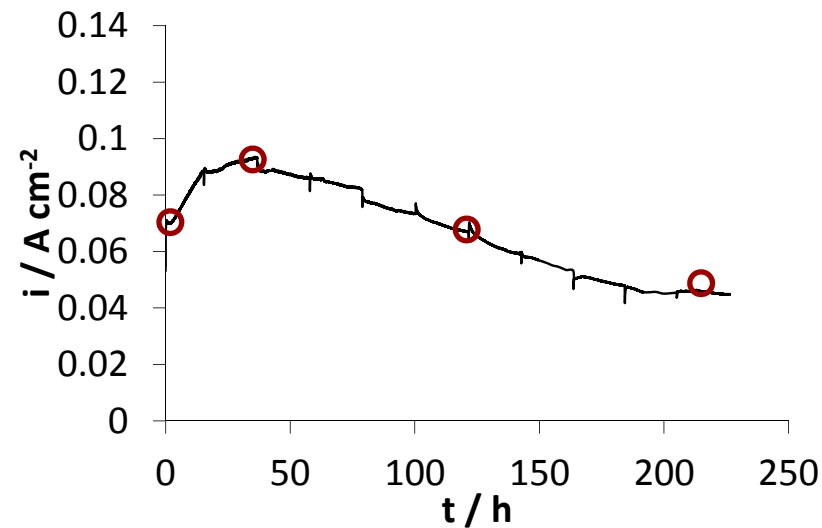
airbrush



electrospray



- ❑ Two different stages: activation and decay
- ❑ Current distribution is uneven and changes significantly during the lifetest
- ❑ No aparent influence of the reagents' inlets and outlets

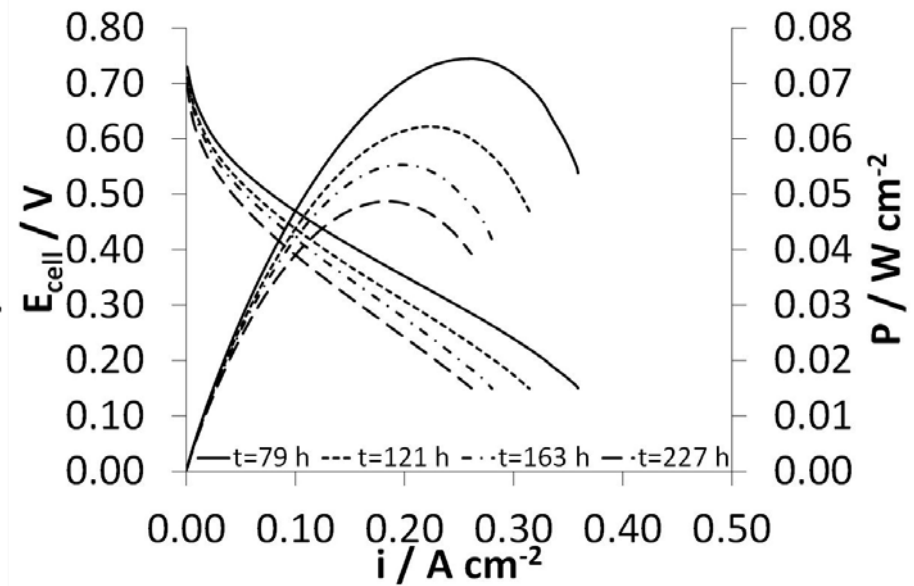
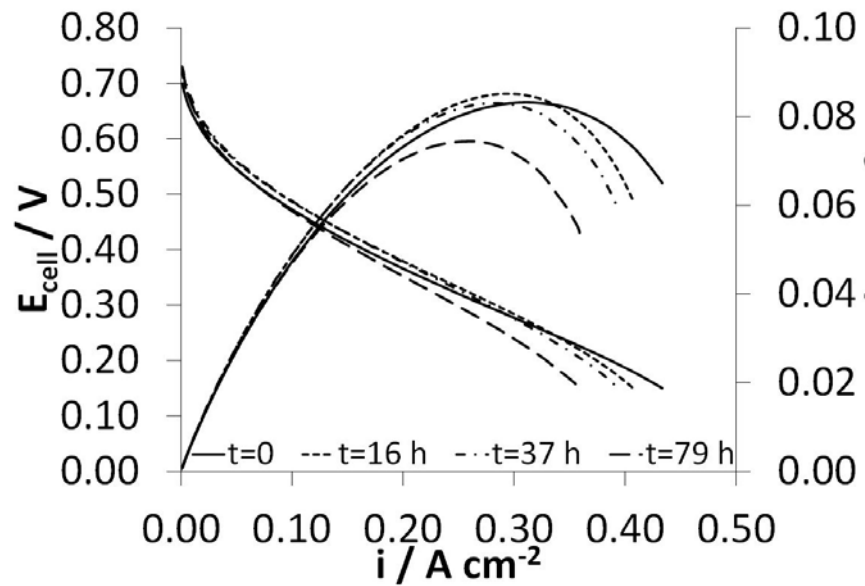


Significant change of the current distribution map during the lifetest.

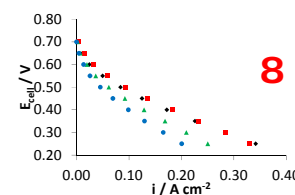
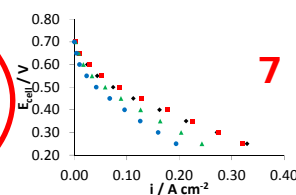
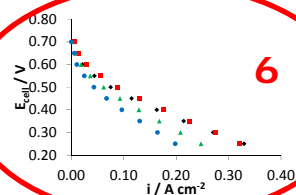
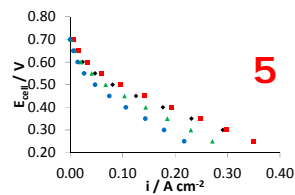
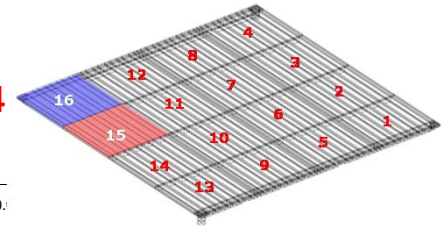
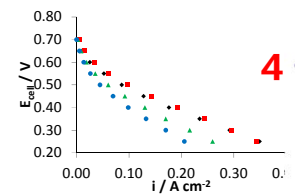
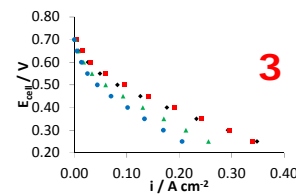
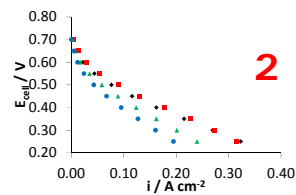
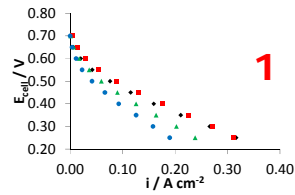
Differences are much higher at the end of the test

Keep in mind that average current decreases in the second state and maps reflects only changes

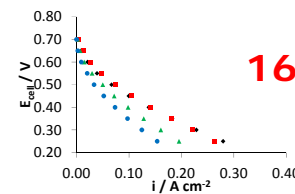
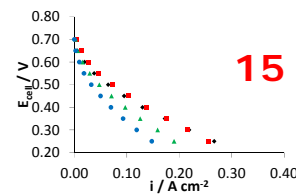
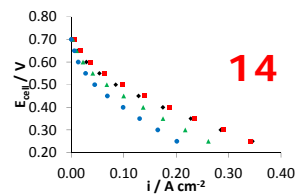
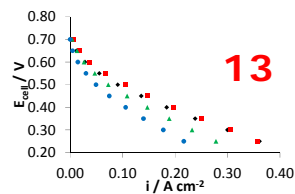
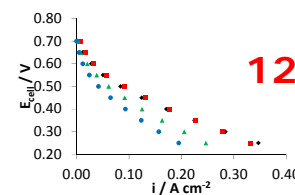
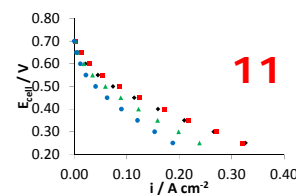
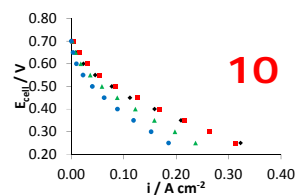
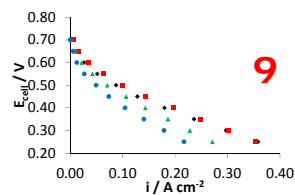
- Global polarization curves

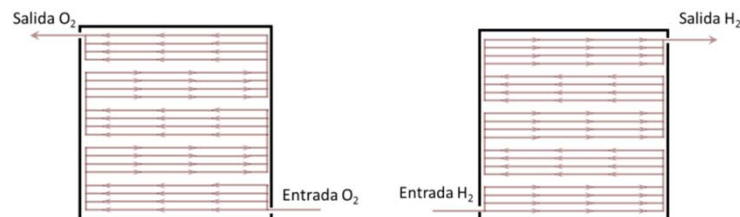
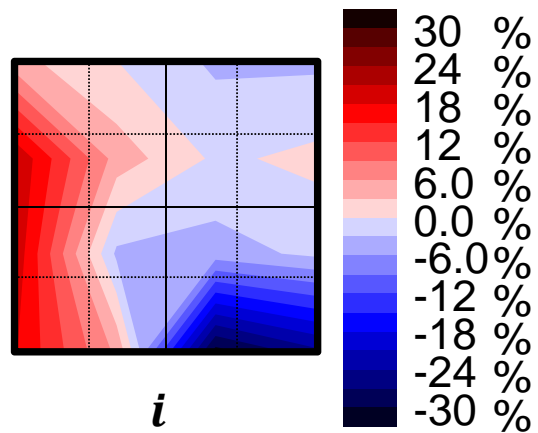
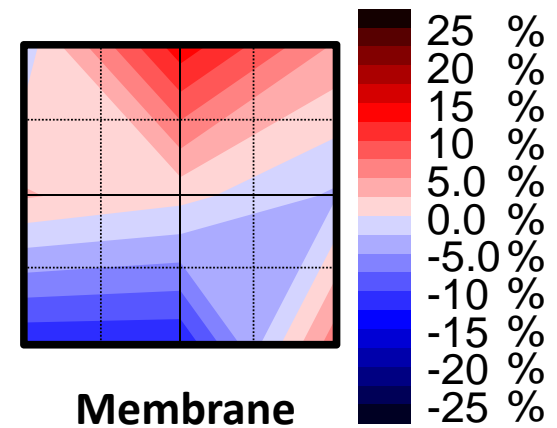
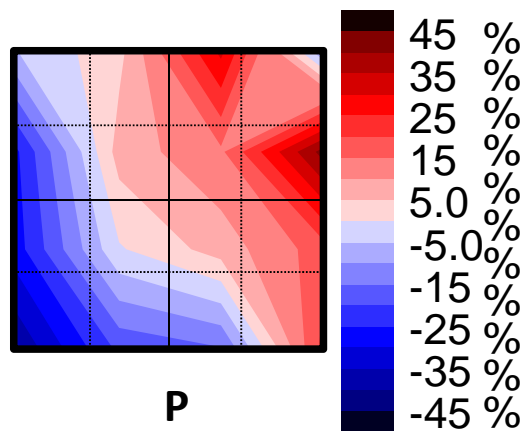
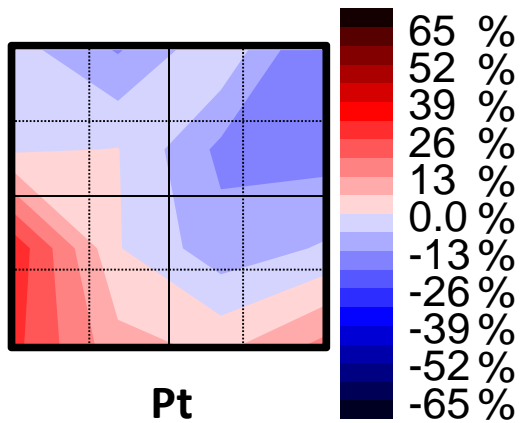


Local polarization curves



- ◆ Experimental t=0h
- Experimental t=37 h
- ▲ Experimental t=121 h
- Experimental t=227 h





- **Catalyst distribution**
 - Electrode manufacturing
 - Particle agglomeration
- **Water distribution**
 - Flooding
- **Temperature distribution**
 - Design
- **Reagent distribution**
 - Mass transport
 - Flow channels
- **Conductivity distribution**
 - Assemblage



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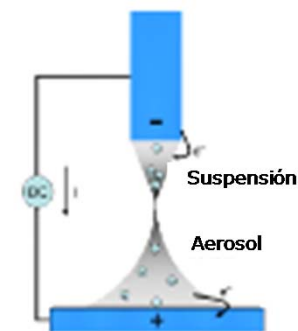
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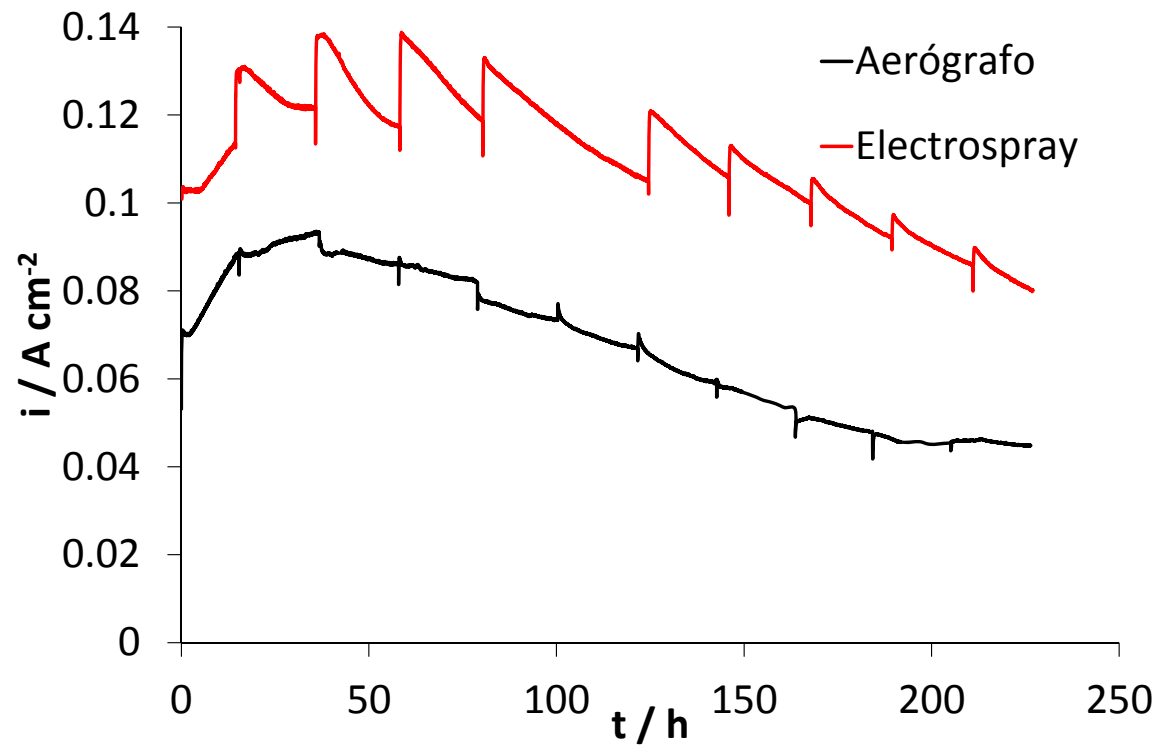
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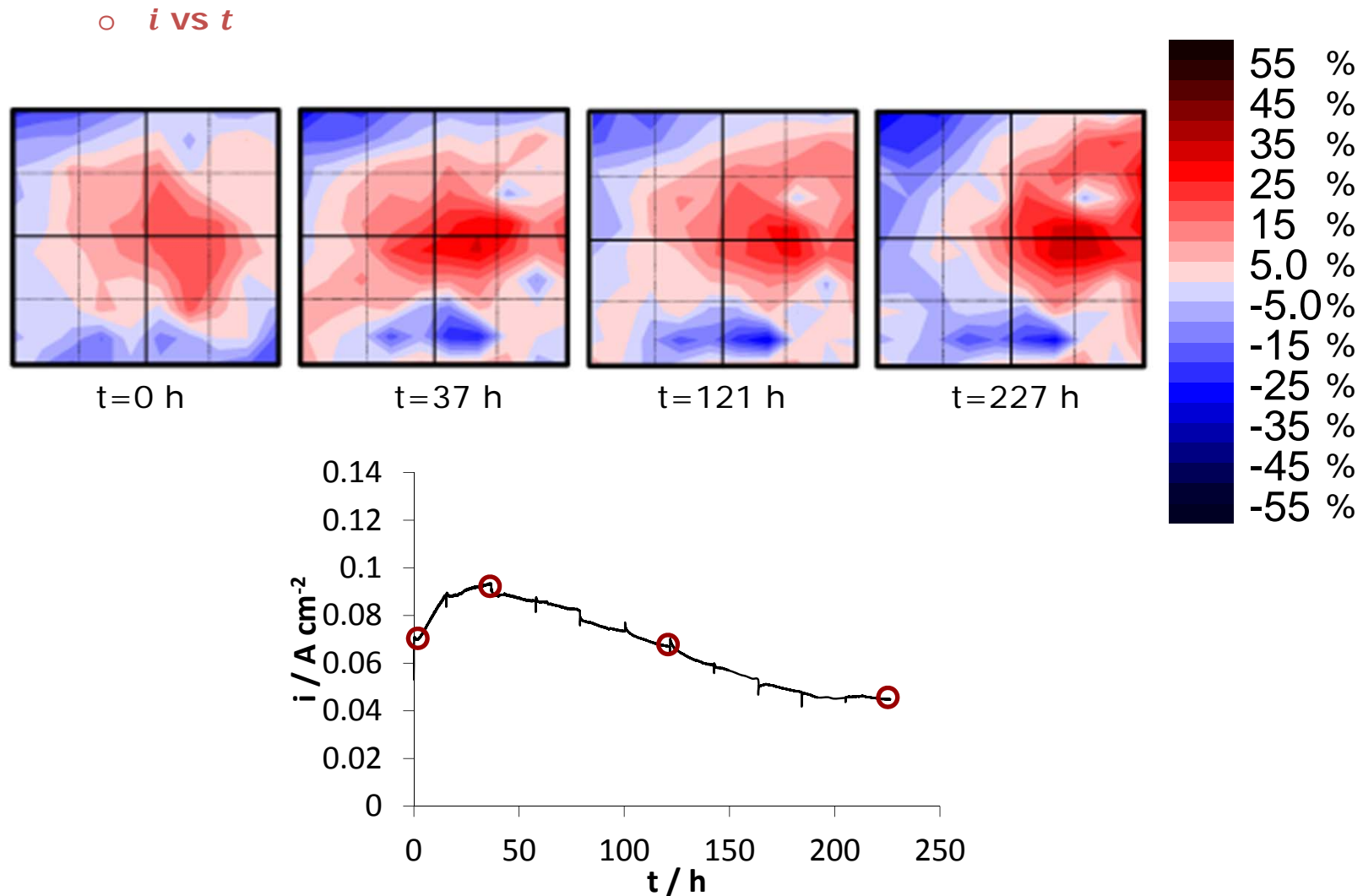
airbrush



electrospray



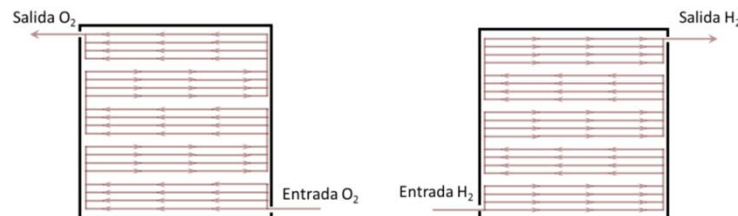
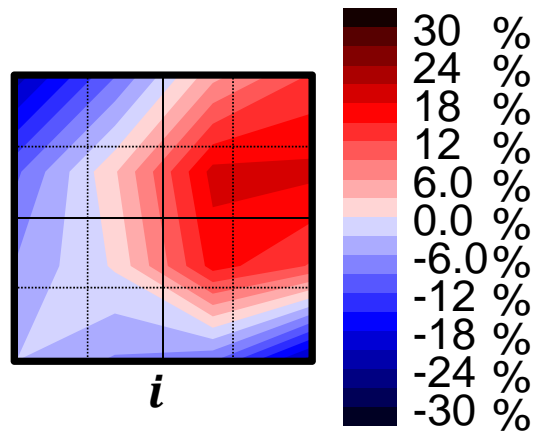
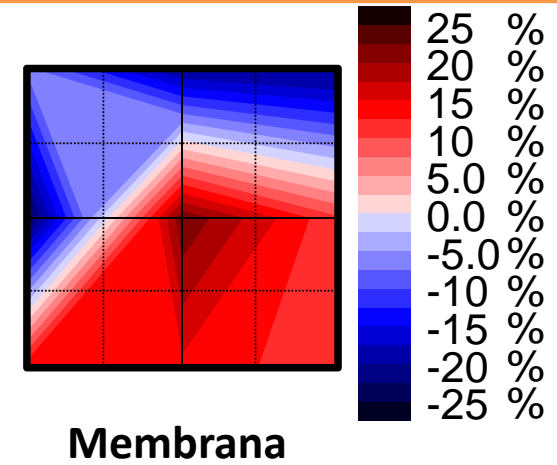
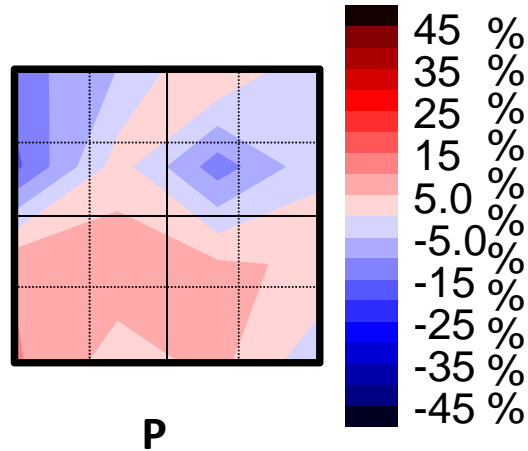
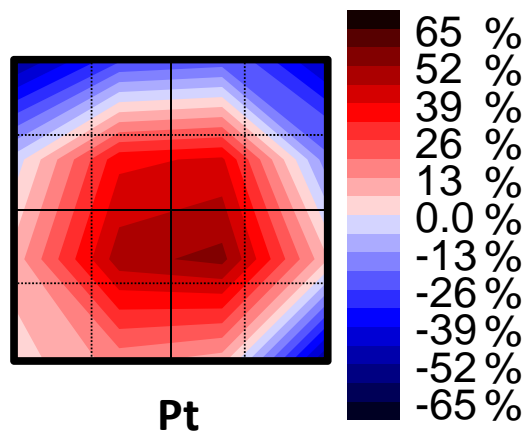
Differences in the current values not in the way in which they change: same stages during the lifetest: activation and decay (no influence of the catalyst deposition technique)



Significant change of the current distribution map during the lifetest.

Differences are much higher at the end of the test

Keep in mind that average current decreases in the second state and maps reflects only changes



▪ Catalyst distribution

- Electrode manufacturing
- Particle agglomeration



▪ Water distribution

- Flooding



▪ Temperature distribution

- Design



▪ Reagent distribution

- Mass transport
- Flow channels



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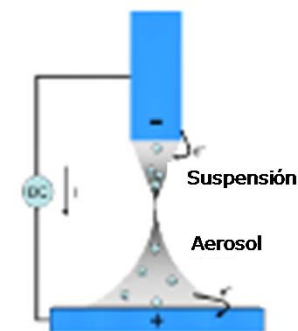
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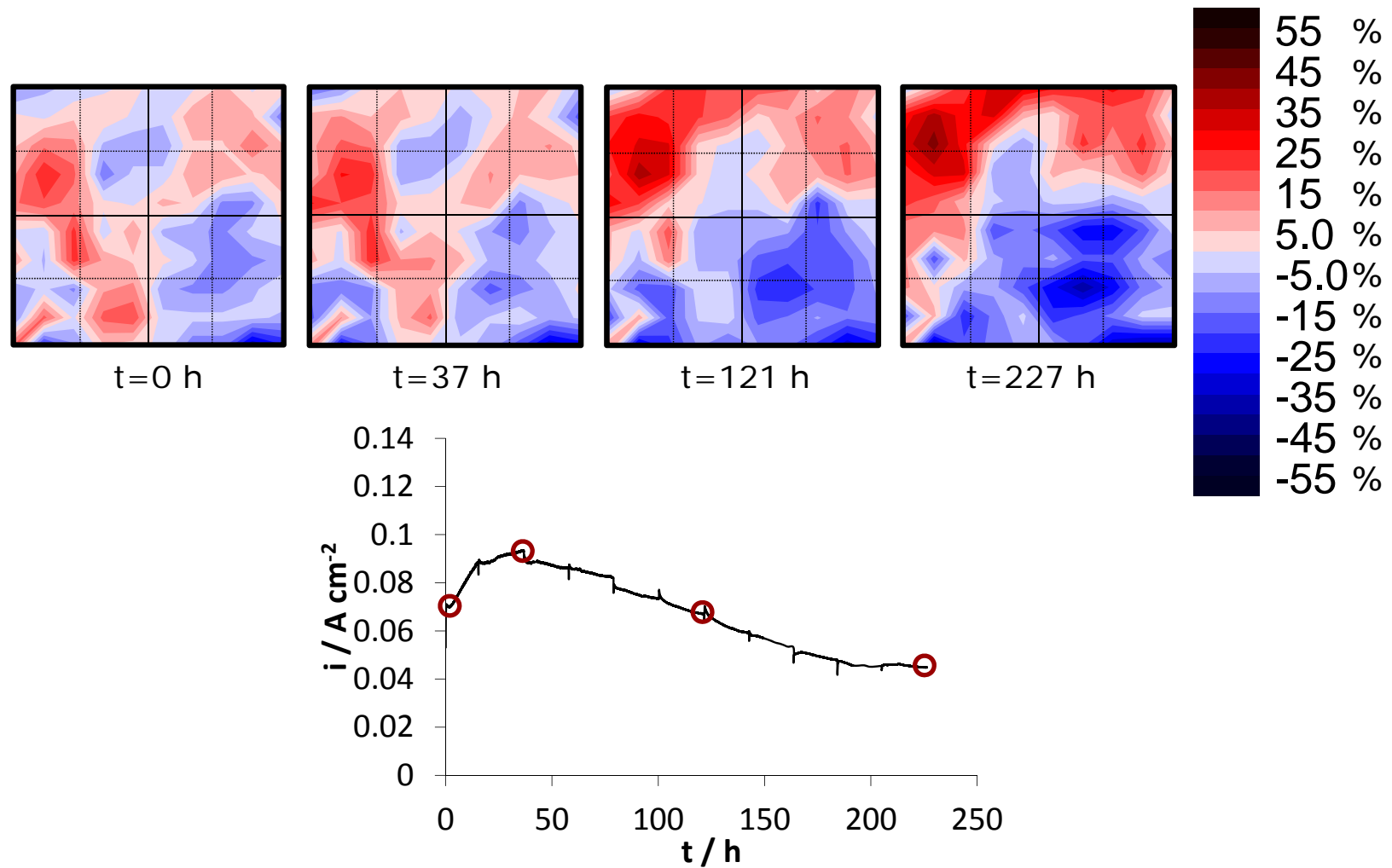
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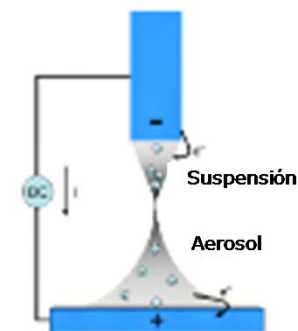
Lifetest III: airbrush; anode: 0.10 mg Pt cm⁻² ; cathode: 0.15 mg Pt cm⁻²

Lifetest IV: electrospray; anode: 0.10 mg Pt cm⁻² ; cathode: 0.15 mg Pt cm⁻²

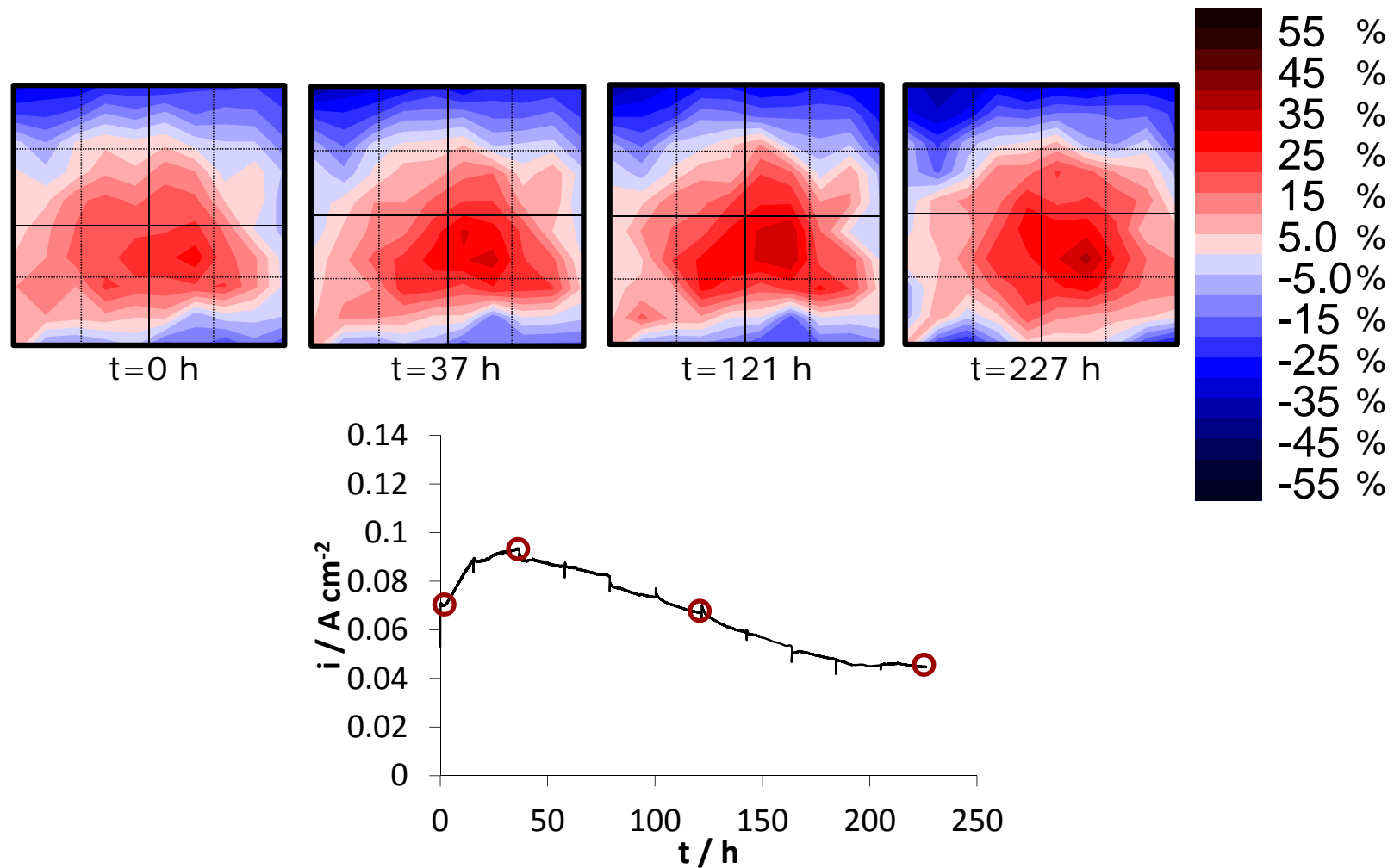
Spread catalytic ink technique:



airbrush



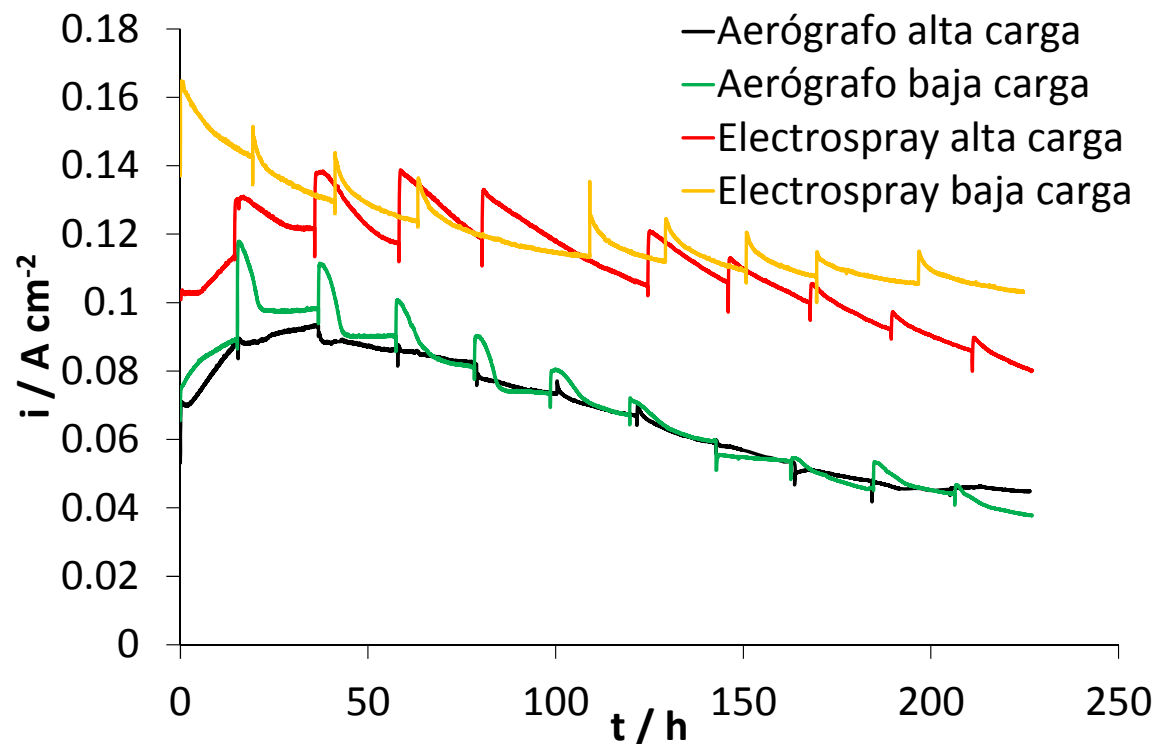
electrospray



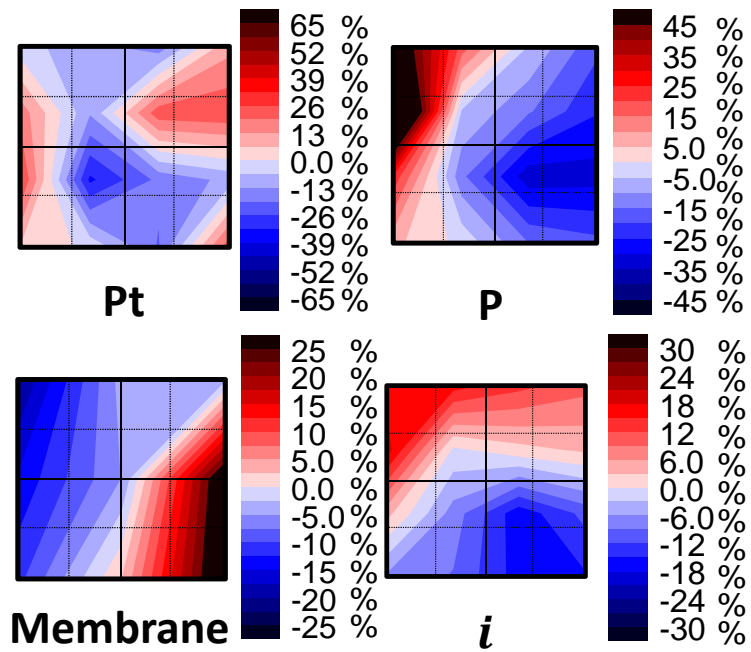
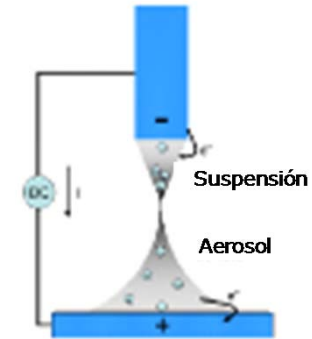
Significant change of the current distribution map during the lifetest.

Differences are much higher at the end of the test

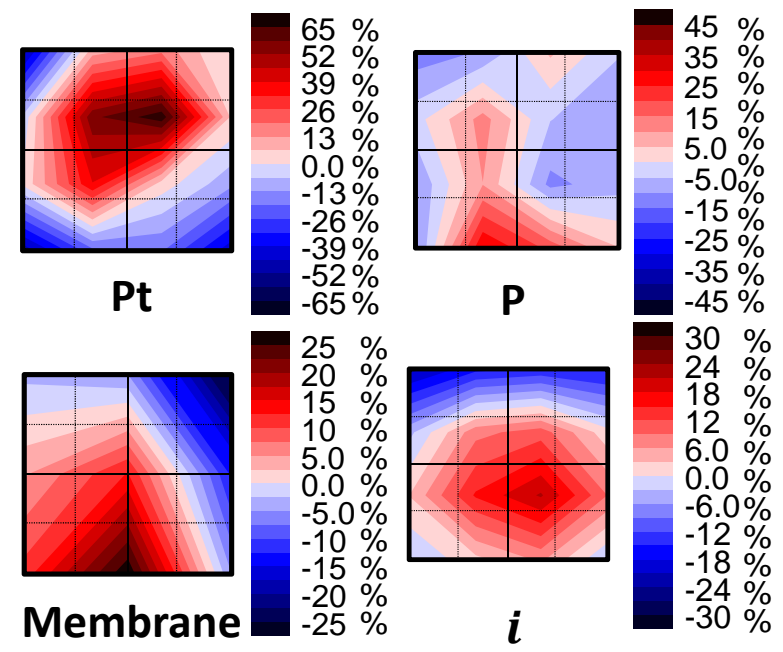
Keep in mind that average current decreases in the second state and maps reflects only changes



Differences in the current values not in the way in which they change: same stages during the lifetest: activation and decay (no influence of the catalyst deposition technique on the deterioration although clearly better results of electropray for the same catalyst content)



☐ No single relationship can be appreciated



☐ Similarities between Pt and i



Introduction

Objetives

Results and discussion

► **Conclusions**

Acknowledgements



Concluding remarks



Manufacture of the components of PBI-HTPEMFC is not difficult but lack of reproducibility associated to the large number of manufacturing steps and the very different nature is inherent to the technology

Composite membranes can help to increase service lifetime and enhance performance

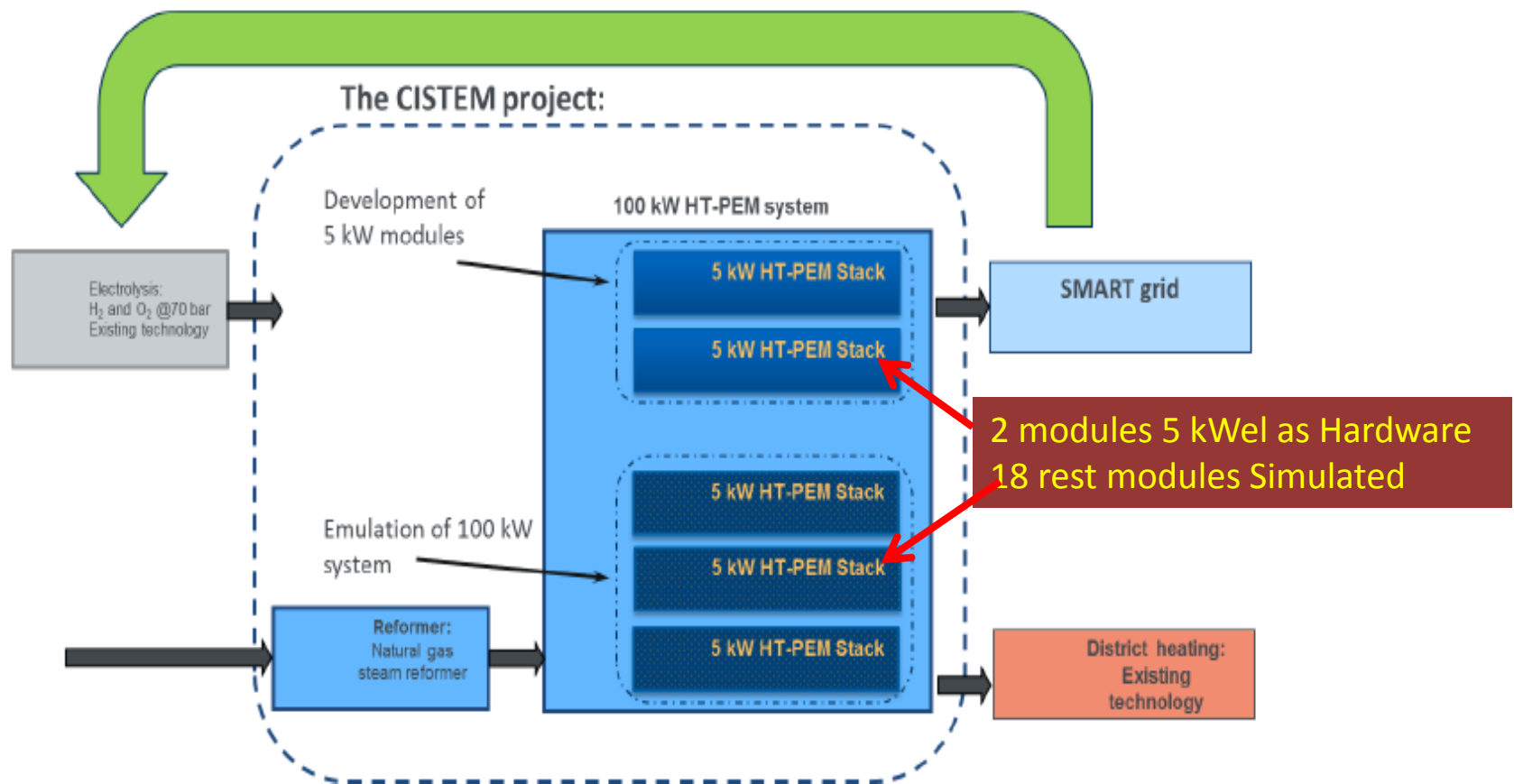
Lifetime and reproducibility remains to be the key drawbacks in PBI-HTPEMFC technology. Non uniform behaviour can not directly be associated to a single parameter (catalyst, reagent distribution, temperature, membrane) to the joint effect of all of them.



Catalyst deterioration is the key to understand PBI-HTPEMFC performance decay . Leaching of phosphoric acid is a much less important problem

New materials beyond state of art are being developed including sulphonated composite PBI Membranes which are showing very interesting results (CISTEM EU project)

CISTEM project: develop a new fuel cell (FC) based CHP technology, which is suitable for fitting into large scale peak shaving systems in relation to wind mills, natural gas and SMART grid applications.





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► **Acknowledgements**



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- The authors further thank the European Commission as part of this work was supported by the Seventh Framework Programme through the project CISTEM (FCH-JU Grant Agreement Number 325262).
- Special thanks to the HYDROGEN DAYS organizers for their kindness and support of the research in hydrogen technology

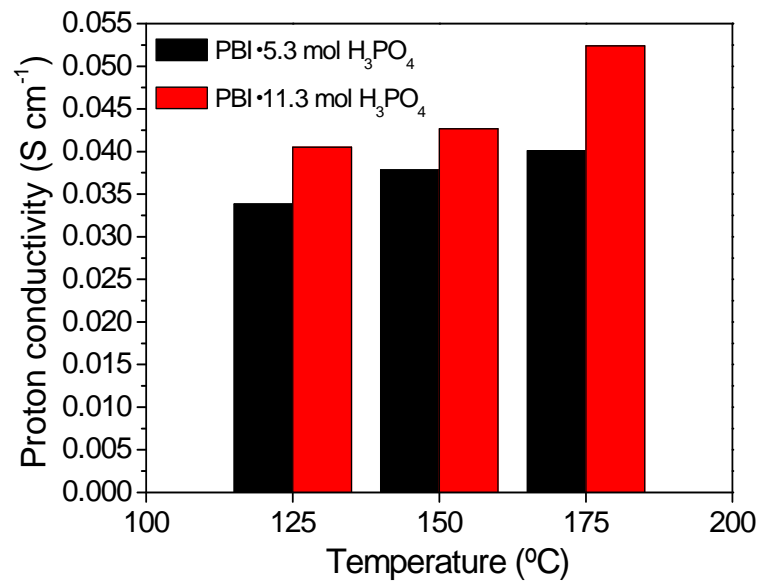




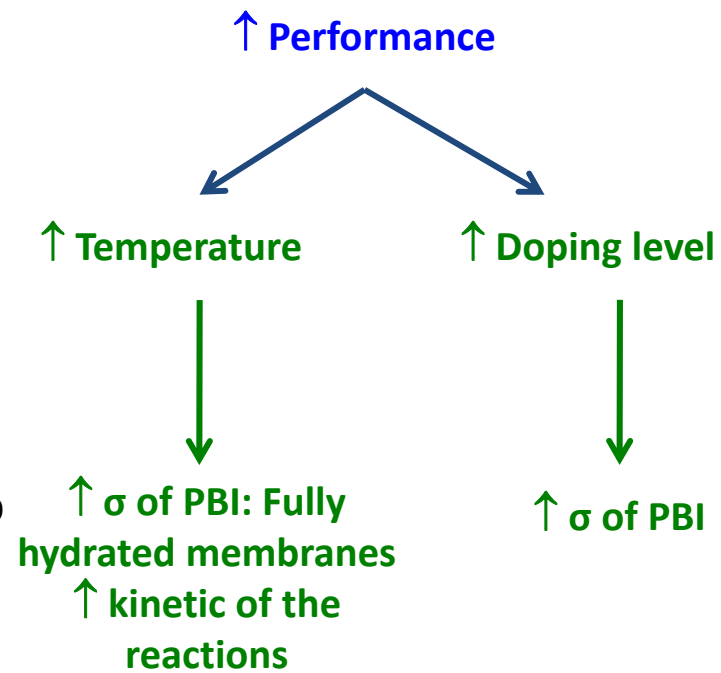
**Thank you for your kind
attention!**

*Composite membranes for high temperature PEM fuel cells:
from single cells to stack. M.A. Rodrigo, J. Lobato, P.
Cañizares, F.J. Pinar, H. Zamora and D. Úbeda*

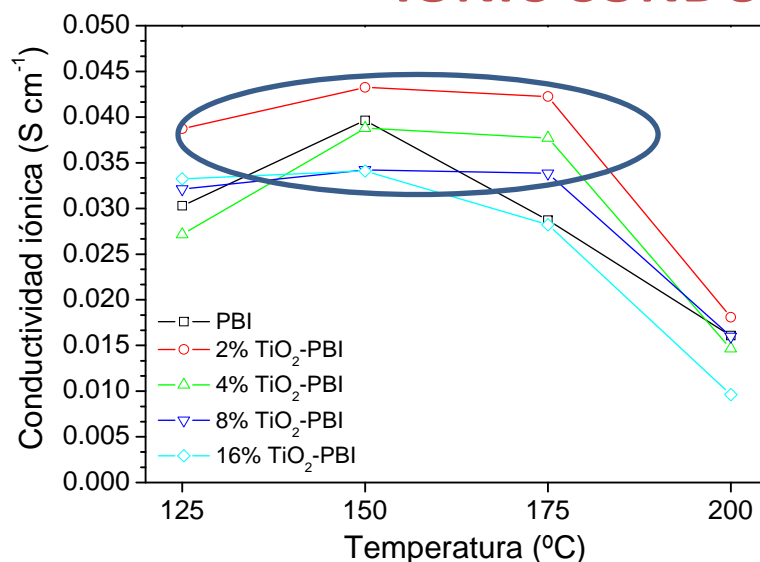




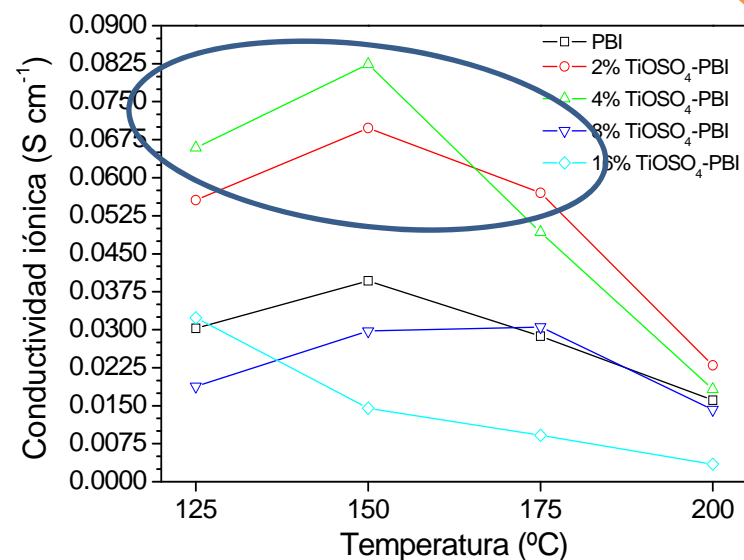
Influence of temperature on proton conductivity of PBI membranes used in fuel cell and doped into different H_3PO_4 bath solutions



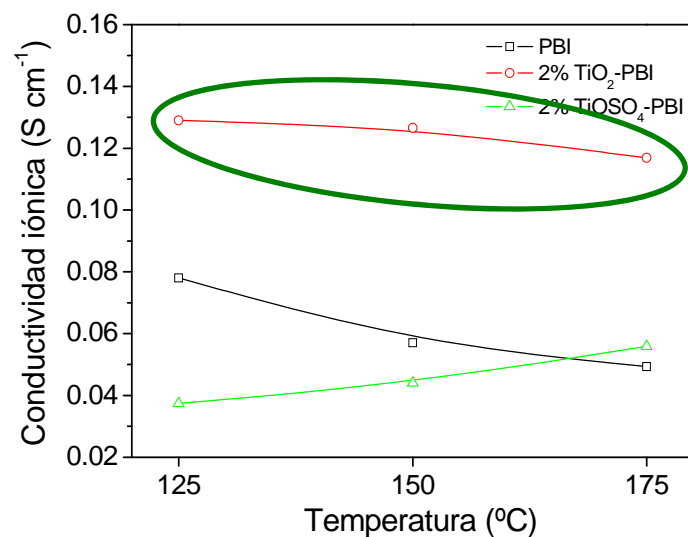
IONIC CONDUCTIVITY



Ionic conductivity for TiO₂ composite PBI membranes and Standart PBI membranes at differents temperatures. [H₃PO₄]= 75 % p/p



Ionic conductivity for TiOSO₄ composite PBI membranes and Standart PBI membranes at differents temperatures. [H₃PO₄]= 75 % p/p



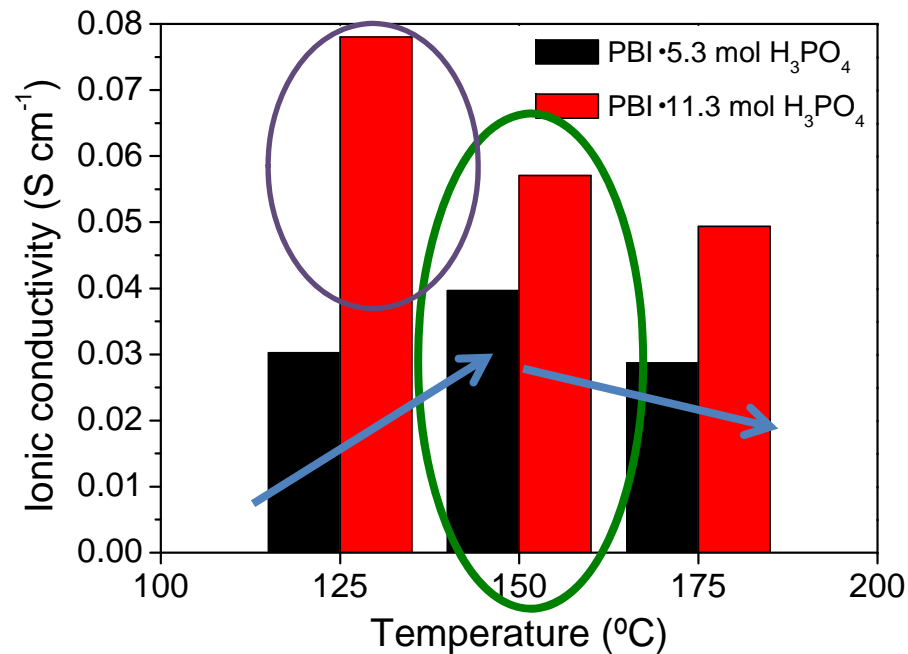
Ionic conductivity of composite and standart membranes based PBI at differents temperatures. [H₃PO₄]= 85 % p/p

Composite membranes → ↓ Decrease in σ with $\uparrow T^a$

2, 4, 8 % TiO₂-PBI and 2, 4 % TiOSO₄-PBI
75 % p/p H₃PO₄ ↓ $\sigma \uparrow$
PBI

2 % TiO₂-PBI → ↑↑ σ
85 % p/p H₃PO₄

IONIC CONDUCTIVITY



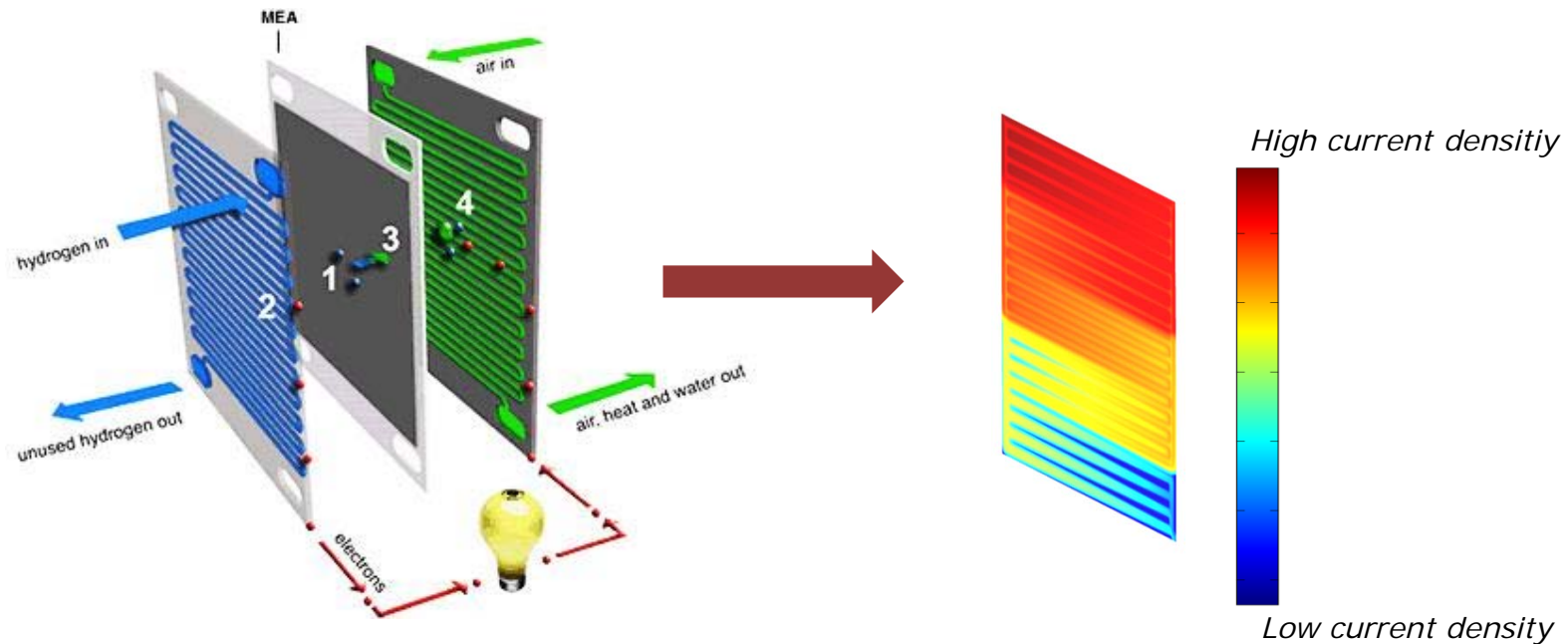
Influence of temperature on ionic conductivity for PBI membranes doped into different H₃PO₄ bath solutions

- ✓ ↑ Acid doping level → ↑ Membrane conductivity → Larger amount of proton carriers (acid and water)
- ✓ ↑ Temperature → ↑ Membrane conductivity → ↑ Mobility of proton "carriers"
- ✓ ↑ 150 °C → ↓ Membrane conductivity → Degradation of H₃PO₄:

$$2 \text{H}_3\text{PO}_4 \rightarrow \text{H}_4\text{P}_2\text{O}_7 + \text{H}_2\text{O}$$
- ✓ PBI·11.3 mol H₃PO₄ → ↑ conductivity at 125 °C → Not totally dehydrated
- ✓ ↓ σ → ↑ Temperature → ↓ Relative Humidity

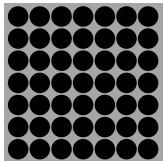
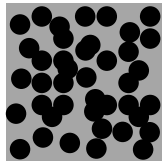

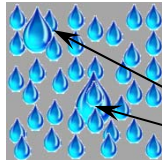


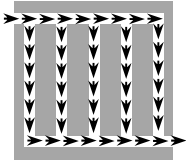
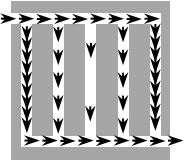


Current density distribution in a PEM fuel cell

- Activation losses → Catalyst properties
- Ohmic losses → Electrolyte properties
- Concentration losses → Reagent concentration



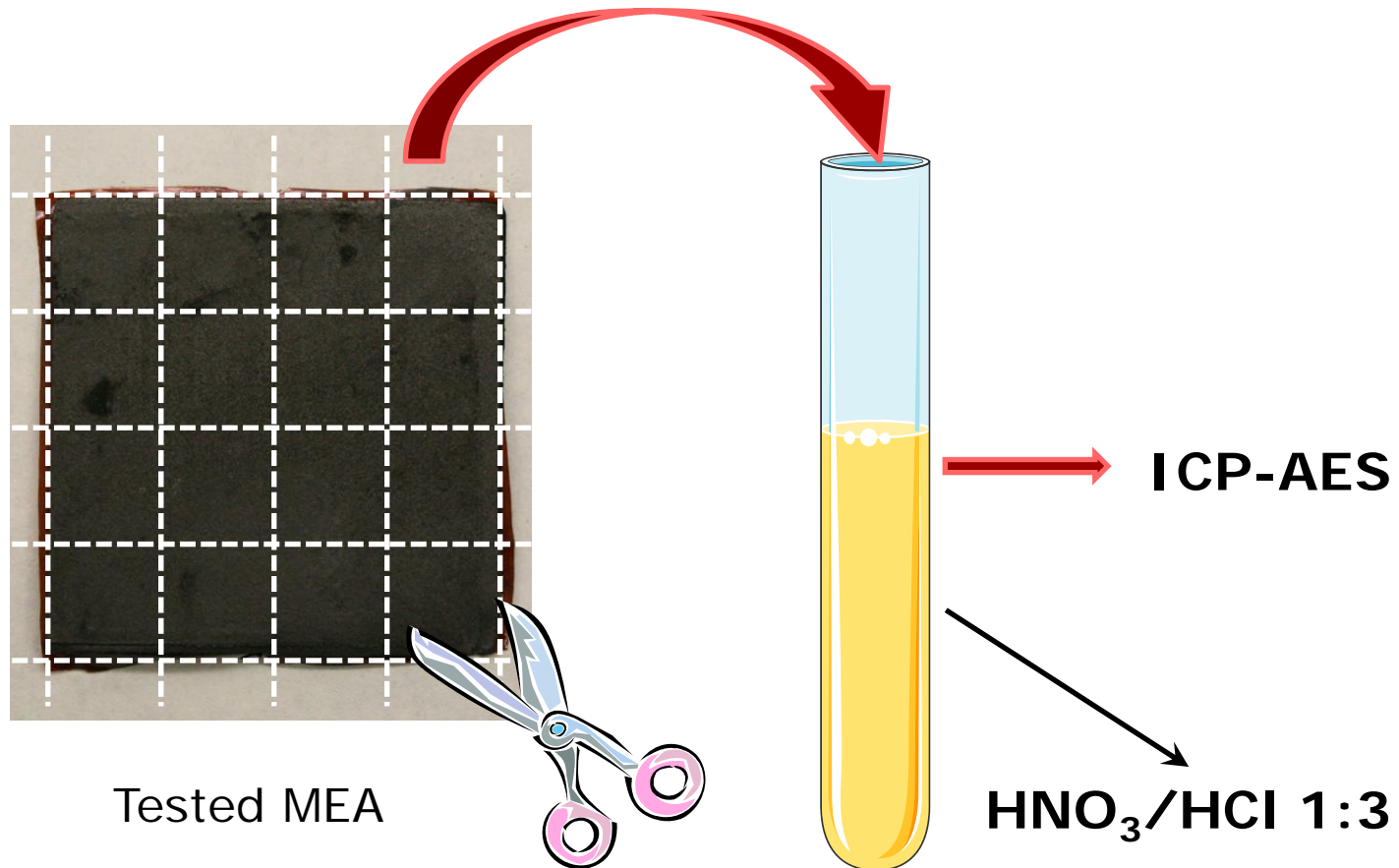
❑ In practice, current density distribution is not uniform

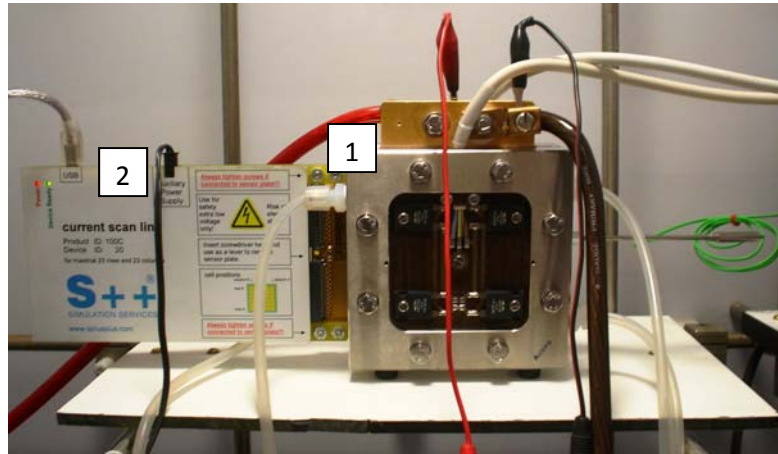
➤ Current density distribution in a PEM fuel cell

	<u>Ideally</u>	<u>In practice</u>
▪ Catalyst distribution <ul style="list-style-type: none">○ Electrode manufacturing○ Particle agglomeration		
▪ Water distribution <ul style="list-style-type: none">○ Flooding		
▪ Temperature distribution <ul style="list-style-type: none">○ Design		 <i>Flooded areas</i>
▪ Reagent distribution <ul style="list-style-type: none">○ Mass transport○ Flow channels		
▪ Conductivity distribution <ul style="list-style-type: none">○ Assemblage		

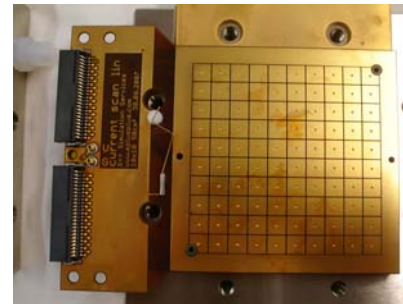
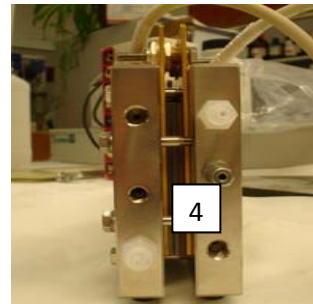
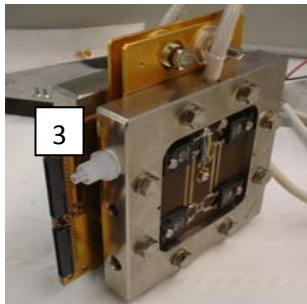
Post-mortem analysis

➤ Analysis of Pt and P content





Element	Description
1	Fuel cell
2	Data acquisition board
3	Sensor plate
4	End plates



- ❑ Array of 10 x 10 sensors. Each sensor measures the electric current flowing through it.
- ❑ Measurement principle: variation of the magnetic permeability